

REINHOLD ENVIRONMENTAL Ltd.



**2013 NO_x-Combustion Round Table
& Expo Presentations**

February 18 & 19, 2013, in Salt Lake City, UT / Hosted by PacifiCorp

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Reinhold Environmental NOx Round Table

February 19, 2013

The Trials and Tribulations of SCR O&M

Presenters:

Noel Rosha and Dr. Greg Holscher

IBIDEN CERAM Environmental, Inc.

+1 913 239 9896

noel.rosha@ceram-usa.com

greg.holscher@ceram-usa.com

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Presentation Topics

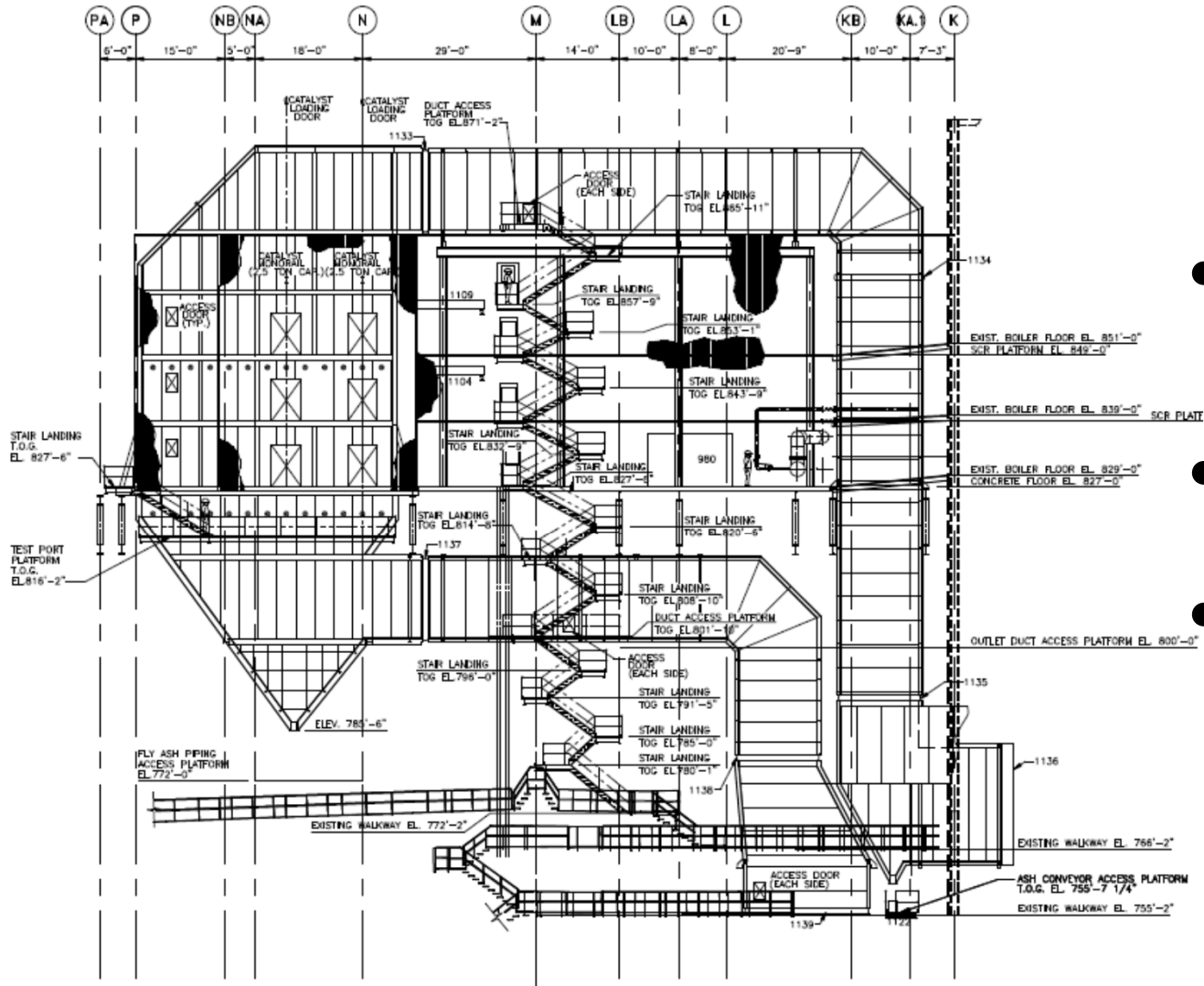
- Xcel Energy A.S. King Plant Case Example – by Noel Rosha
 - Unit and SCR Overview
 - DeNOx Demand and Reactor Potential
 - SCR Operations and Performance
 - Catalyst Management Planning Beyond Guarantee Life
- NIPSCO Bailly Unit 8 Case Example – by Greg Holscher
 - Unit and SCR Overview
 - Reactor Inspection Review
 - CFD Modeling Review
 - Affects of System Modifications to AIG Tuning
 - Summary

Xcel Energy A.S. King Unit 1

- 588 MW in service beginning 1968
- PRB coal fired
- B&W cyclone boiler
- 2004 – 2007 Rehabilitation Project
 - Steam turbine replacement
 - Steam generator overhaul
 - AQC additions
- SCR in service beginning 2007



A.S. King Unit 1 SCR Design



- B&W Cyclone Boiler
- High Dust SCR
- 2+1 Layer Arrangement

ELEVATION LOOKING NORTH

Original Catalyst Supply (By Others)

NOx Reduction	89% (0.74 to 0.08 lb/Mbtu)
SO₂ to SO₃ Conversion Rate	0.5% per Layer (1% for 2 Layers)
Honeycomb Catalyst Pitch	7.1 mm (21 x 21 cell)
Catalyst Length	1,315 mm
Module Arrangement per Layer	13 x 11
Design Catalyst Deactivation Rate	K/Ko = 0.73 after 24,000 hrs Equiv. K/Ko = 0.78 after 16,000 hrs

Xcel Energy King Plant SCR Key Concerns

- 1) Aggressive Catalyst Design by Supplier
 - 7.1 mm Pitch Catalyst (Very Aggressive for PRB)
 - Aggressive Catalyst Deactivation Rate Assumption (0.73 K/Ko at 24,000 hr)
- 2) Small Pitch →→ 35% Catalyst Pluggage (5% Was Design)
- 3) Result was 2 Initial Catalyst Layers (2+1 Reactor)
 - Operates as 3+0 With More Frequent Changeouts
 - Proper Catalyst Design Would have Required a 4-Layer Reactor

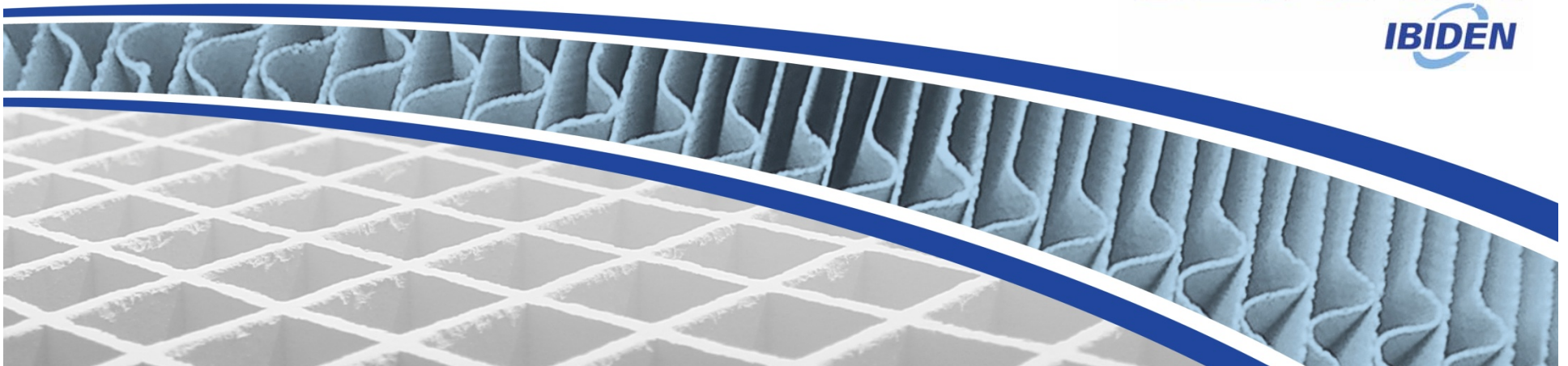
1 + 2 + 3 = Very high ammonia slip and frequent catalyst changeouts

SCR Conditions as of 2010

- **NH₃ Slip of ~30 ppm** measured in June 2010 after ~20,000 hours
- Pluggage estimated to be >30%
- Emergency **summer 2010 outage** required to install the third layer of catalyst
- CERAM begins discussing catalyst management services with King Plant
- King Plant begins catalyst procurement to replace the existing top layer
- CERAM begins developing a catalyst management plan to achieve King's desired 2-year catalyst layer changeout cycle

DeNOx Demand and Reactor Potential

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Reactor Potential

$$P = K / Av$$



P = Reactor Potential

K = Catalyst Activity, Nm³/m²h or Nm/h

Av = Area Velocity, Nm/h

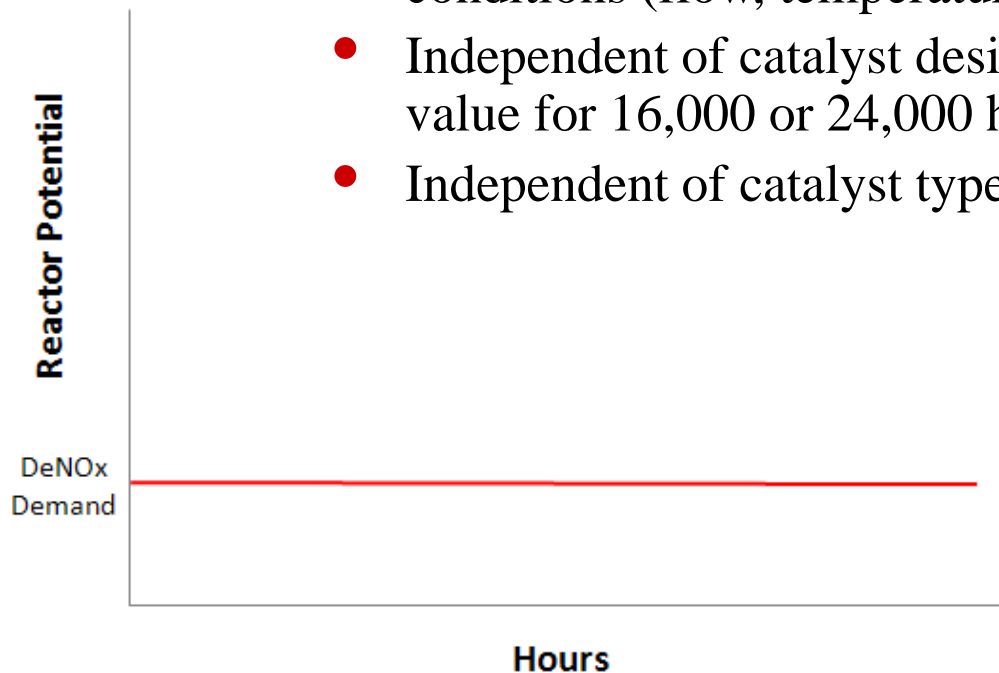
(normal gas flow, Nm³/h divided by total installed catalyst surface area, m²)



The Magnitude of Reactor Potential Determines
the Amount of SCR System Performance Possible
(DeNOx & Ammonia Slip Control)

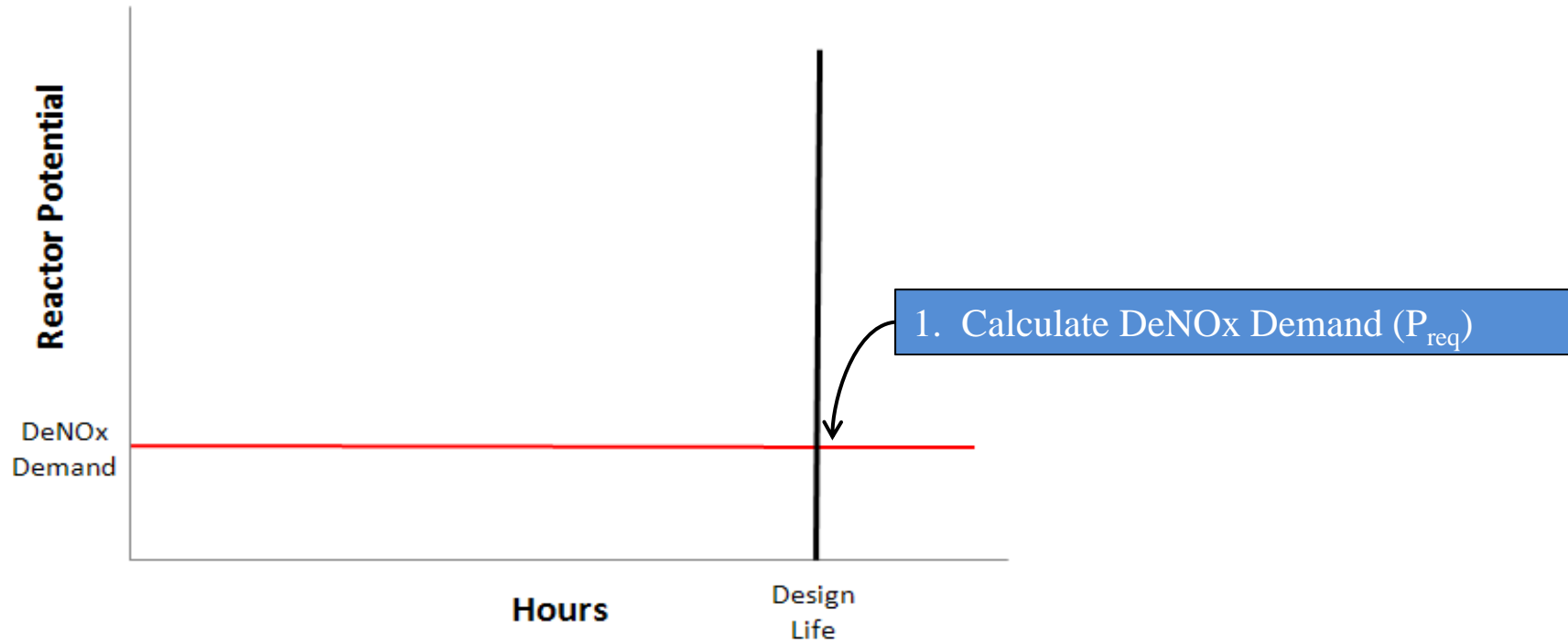
DeNOx Demand

- DeNOx Demand = The reactor potential required to meet NOx removal requirements at the specified operating conditions
- *Calculated* based on NO_x removal requirements, NH₃ slip, and boiler operating conditions (flow, temperature, pressure, etc.)
- Independent of catalyst design life (i.e. same value for 16,000 or 24,000 hour catalyst lives)
- Independent of catalyst type or manufacturer



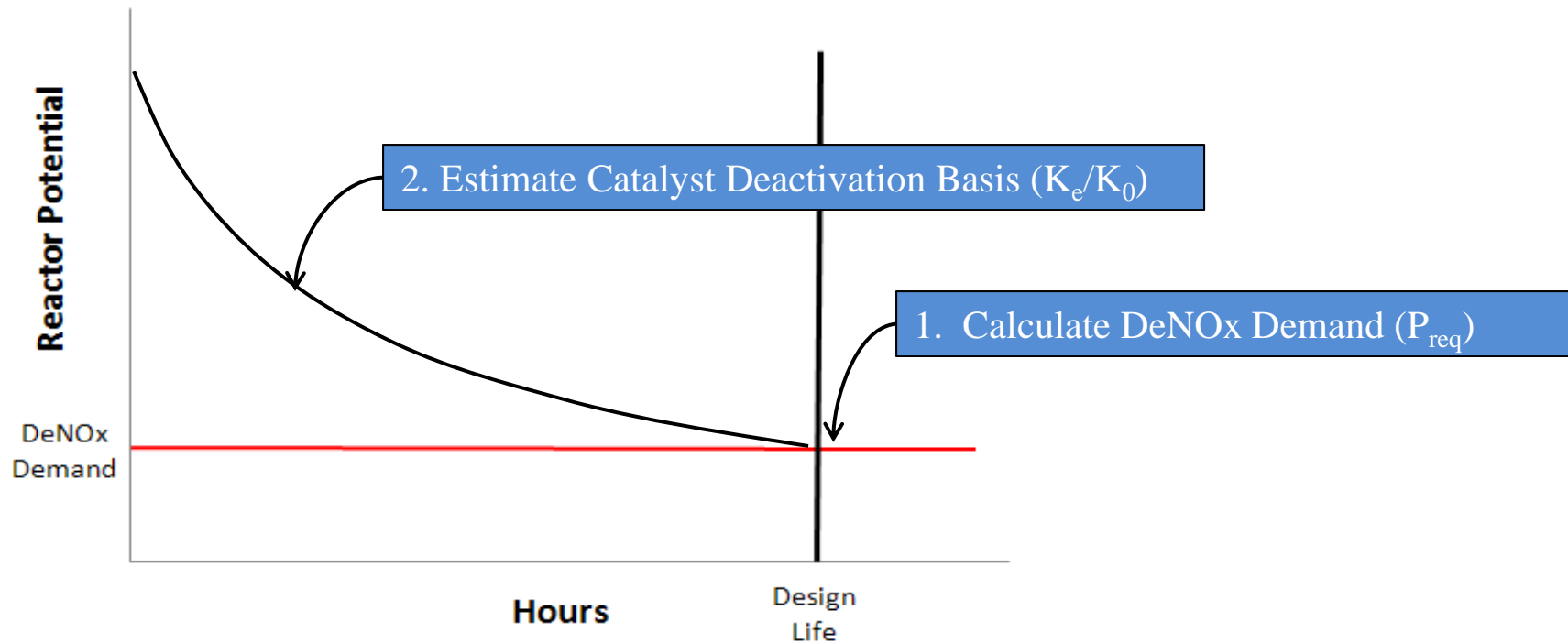
$$P_{req} = K_{req} / Av$$

Catalyst Design Process



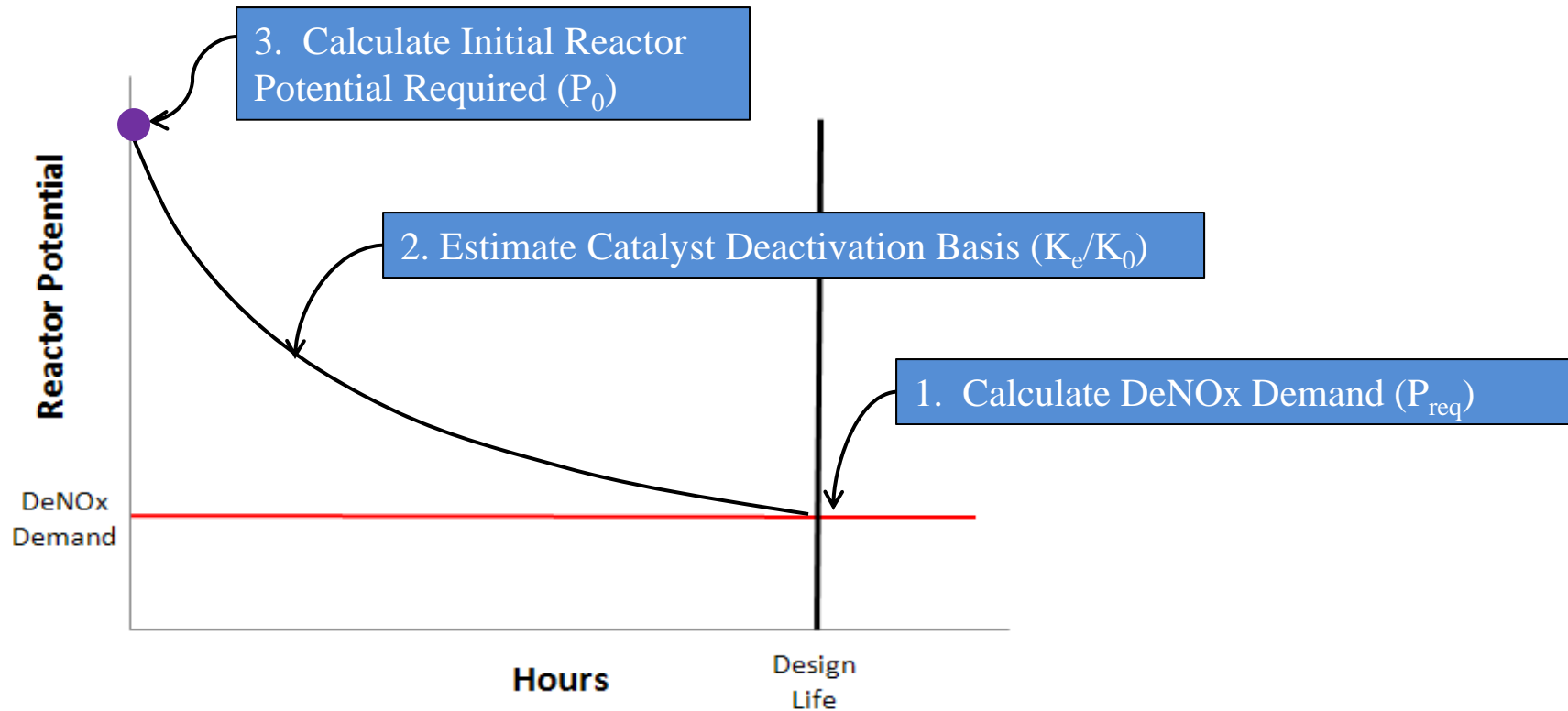
1. Calculate DeNOx demand (P_{req}) required

Catalyst Design Process



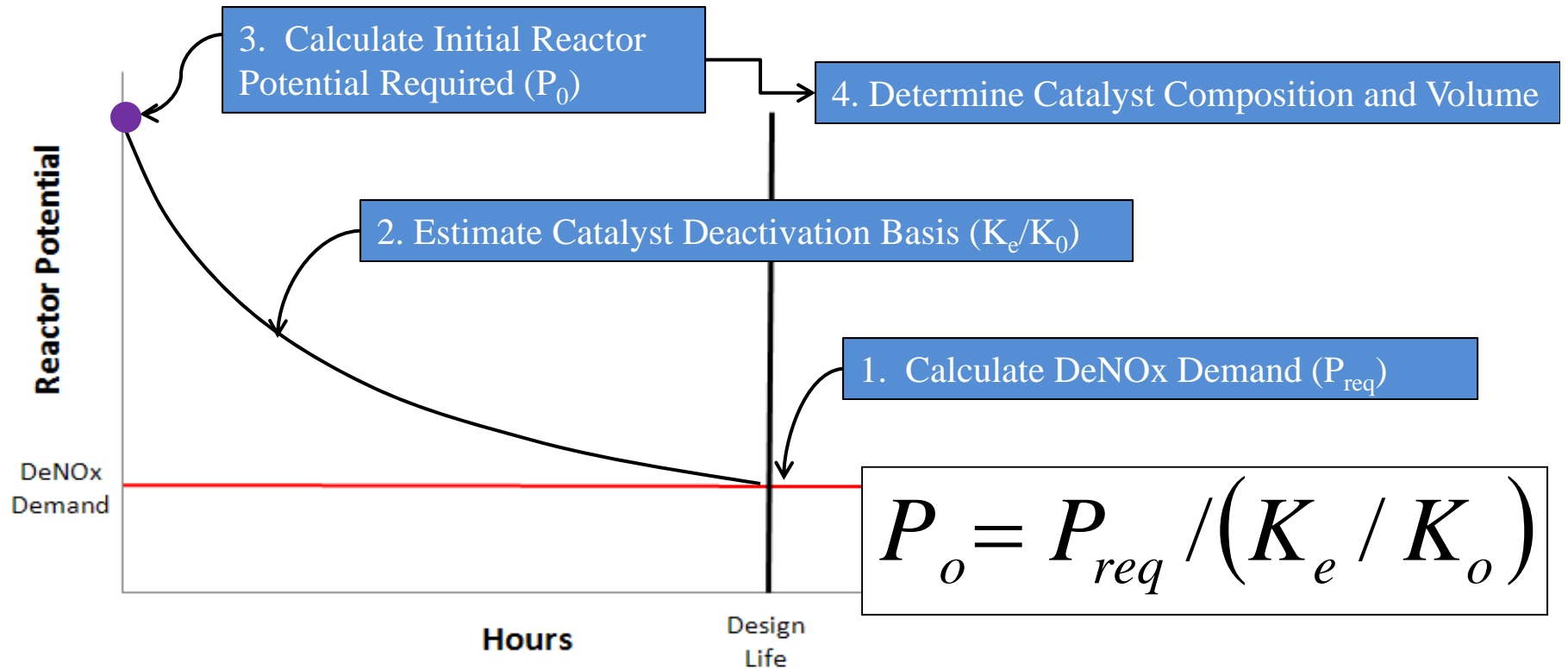
1. Calculate DeNOx demand (P_{req}) required
2. Estimate catalyst deactivation basis (K_e/K_0) based on fuel quality, combustion practices, unit duty, and design life

Catalyst Design Process



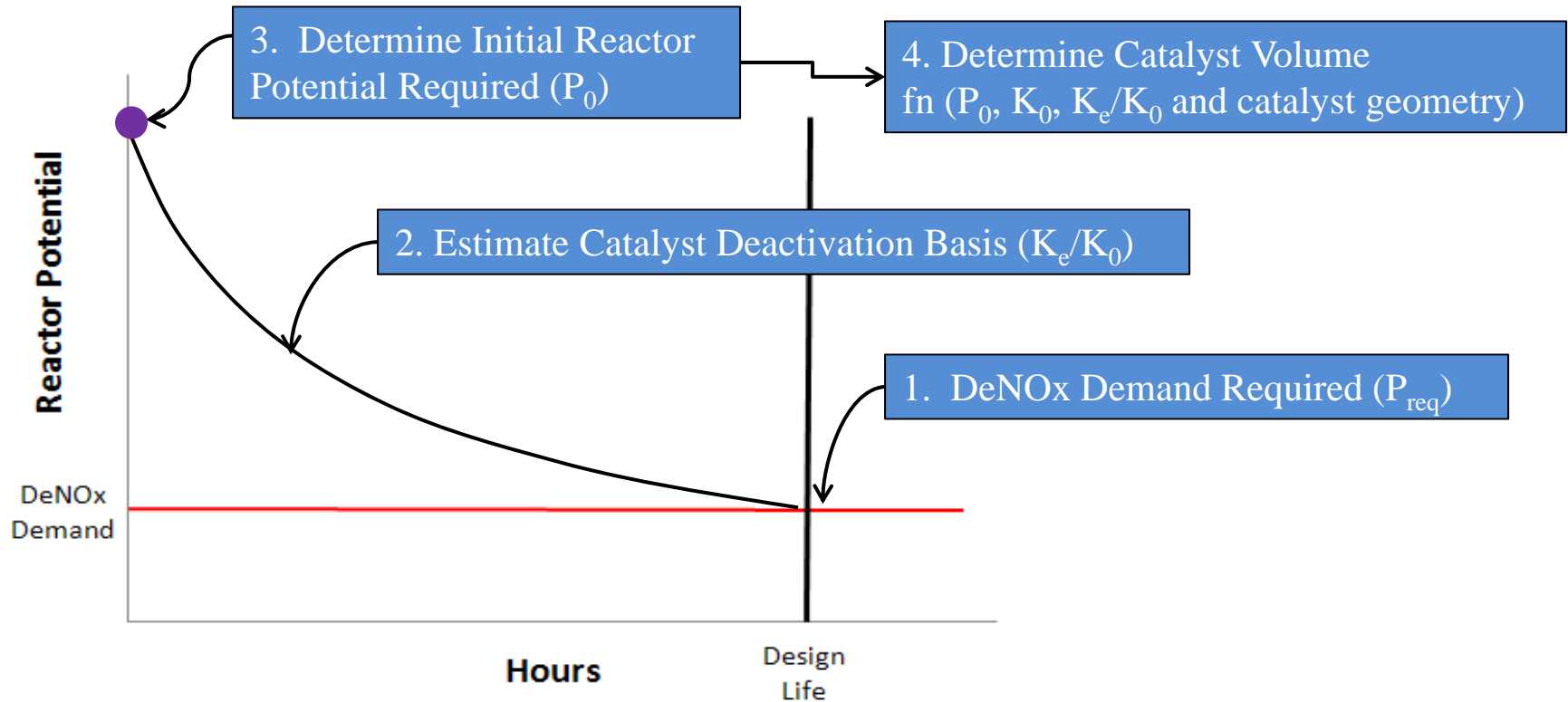
1. Calculate DeNOx demand (P_{req}) required
2. Estimate catalyst deactivation basis (K_e/K_0) based on fuel quality, combustion practices, unit duty, and design life
3. Calculate initial reactor potential [$P_0 = P_{req}/(K_e/K_0)$]

Catalyst Design Process



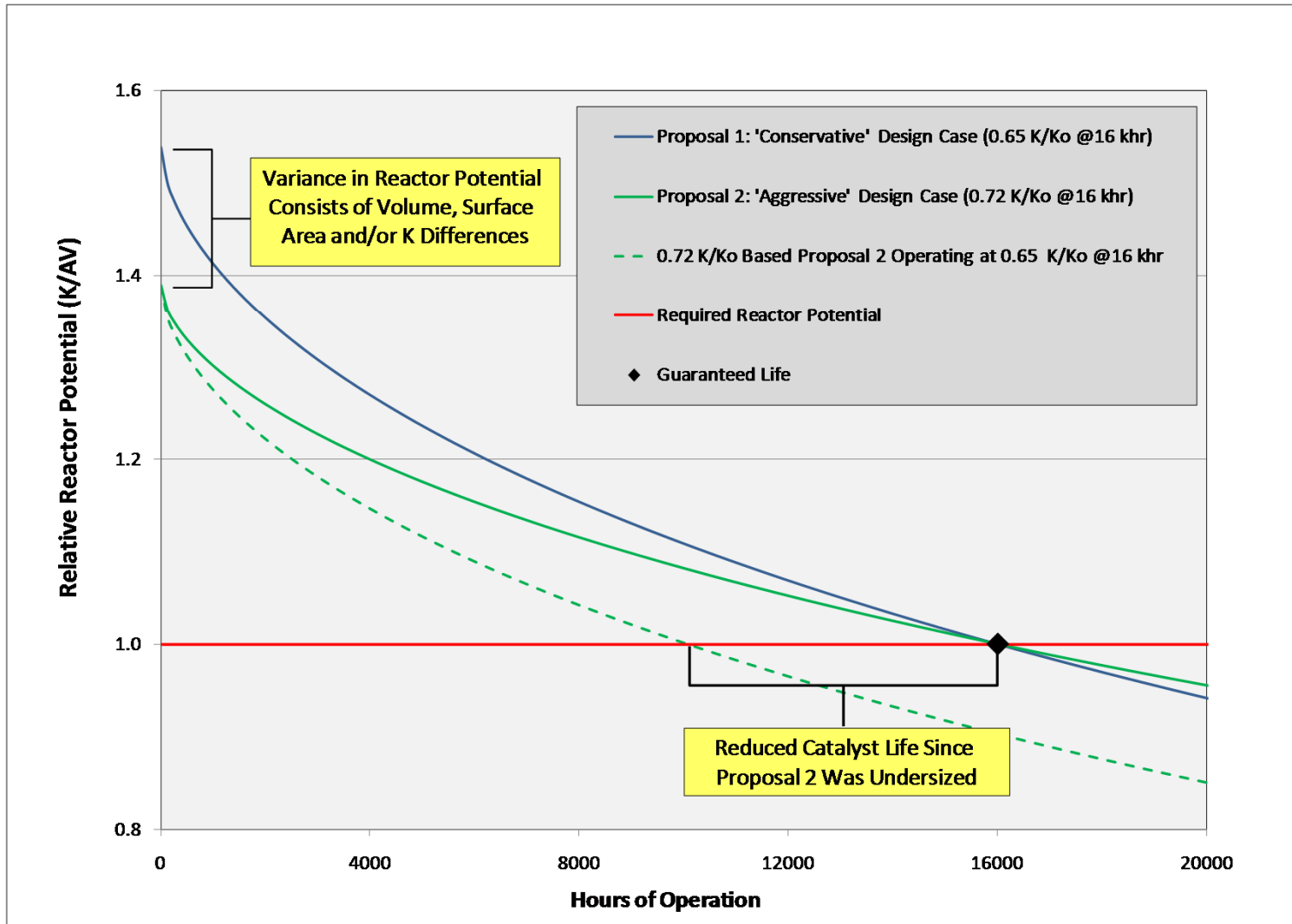
1. Calculate DeNOx demand (P_{req}) required
2. Estimate catalyst deactivation basis (K_e/K_0) based on fuel quality, combustion practices, unit duty, and design life
3. Calculate initial reactor potential [$P_0 = P_{req}/(K_e/K_0)$]
4. Catalyst volume determined based on P_0 , SO₂:3 conversion rate requirement, and catalyst geometry

It is Essential That Initial Catalyst Design Consider a Reasonable Catalyst Deactivation Assumption



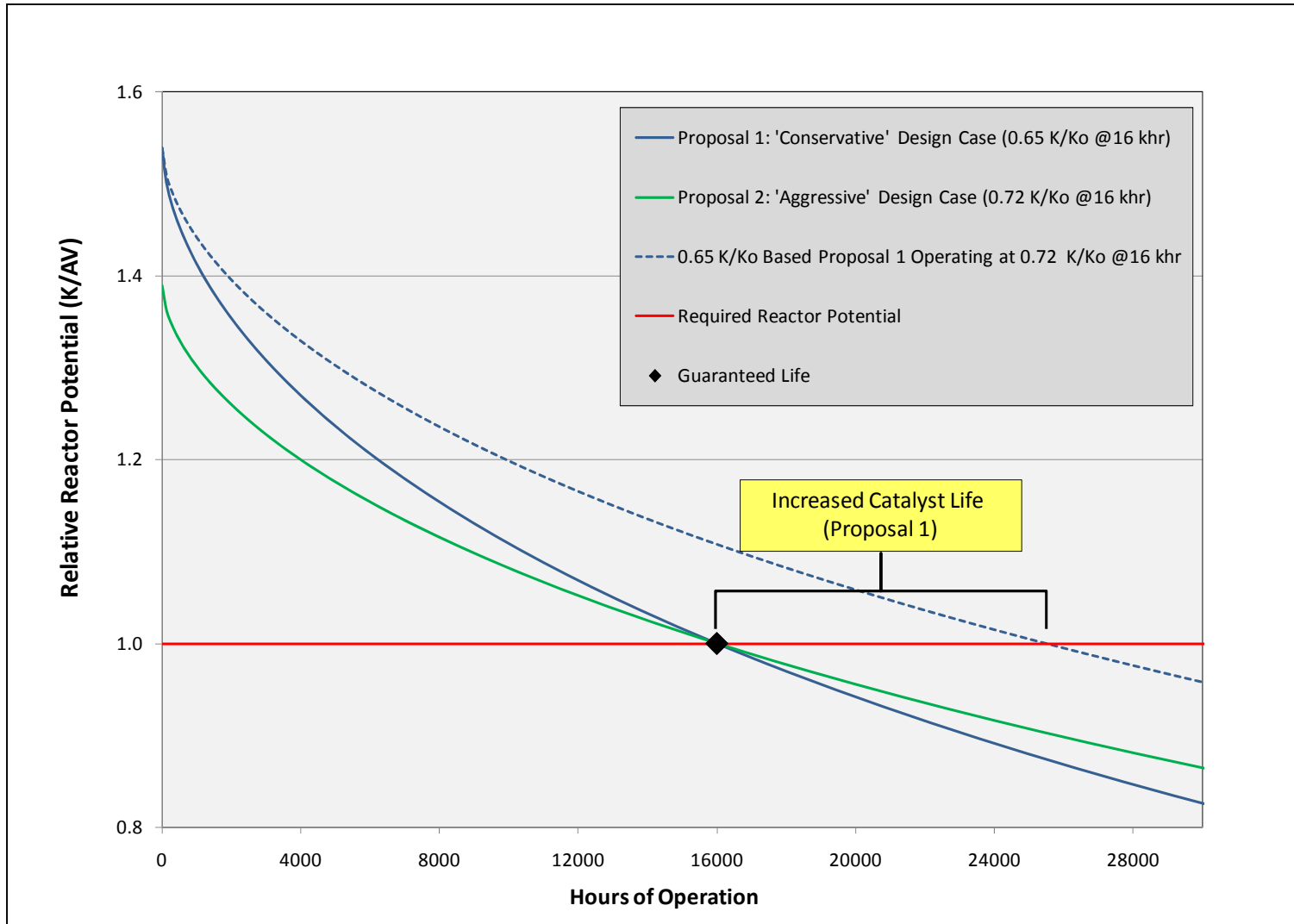
- Examples Will Help Illustrate the Importance of the Catalyst Deactivation Rate Assumption

Catalyst Design Comparison – Case 1 High Deactivation



- A Catalyst Designed for a Deactivation Rate $K/K_o = 0.72$ @ 16khr Will Require a Catalyst Addition at Approximately 11,000 Hours if a Deactivation Rate $K/K_o = 0.65$ Occurs (see dashed line above)

Catalyst Design Comparison – Case 2 Low Deactivation

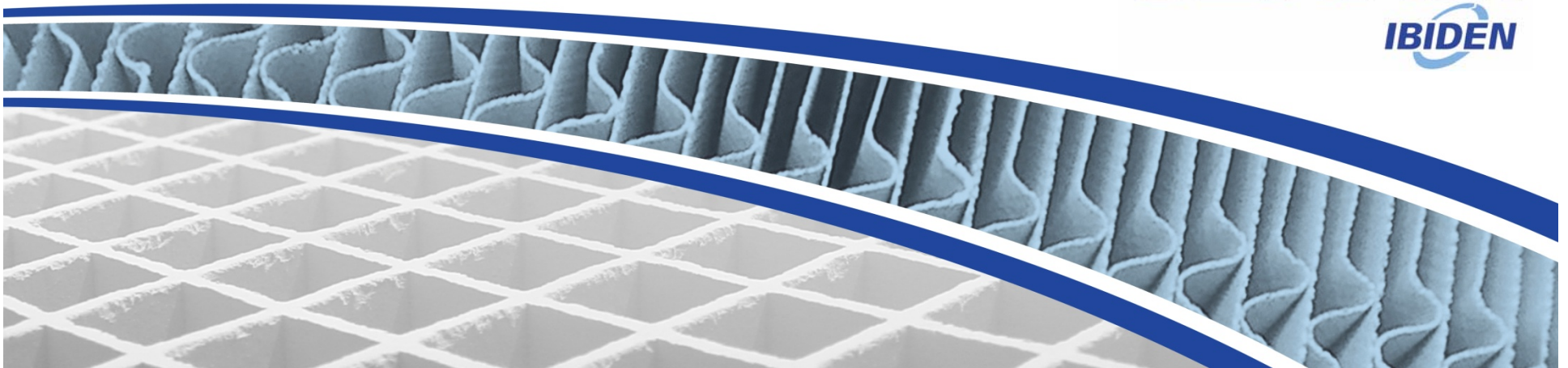


- A Catalyst Designed for a Deactivation Rate $K/K_o = 0.65$ @ 16khr Will Not Require a Catalyst Addition Until Approximately 26,000 Hours if a Deactivation Rate $K/K_o = 0.72$ Occurs (see dashed line above)

A.S. King Unit 1

SCR Operations and Performance

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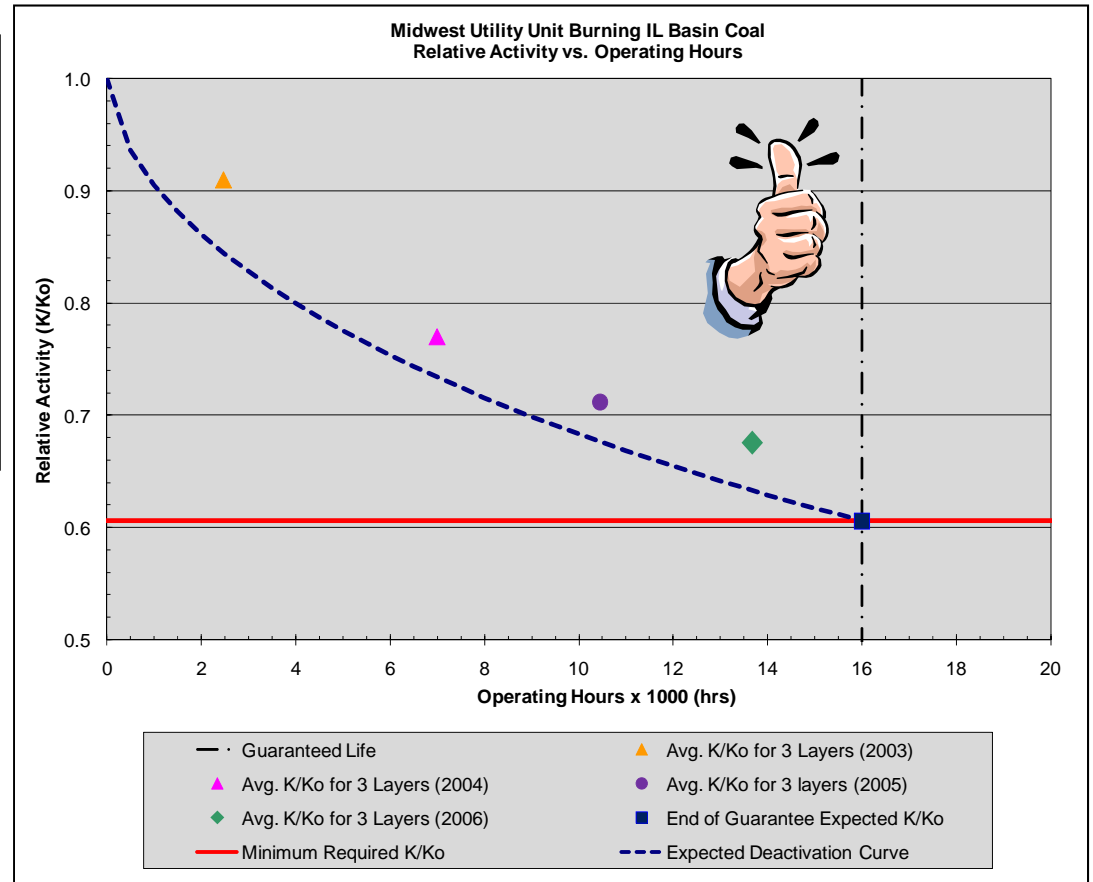


Traditional Catalyst Management

- Utility Pulls Test Elements
- Test Elements Sent to Laboratory
- Laboratory Tests Elements
- Laboratory Indicates if K/Ko is Above Original Sizing Basis
- Is This Catalyst Management Planning?

This Approach:

- Neglects Reactor Mechanical Condition
- Neglects SCR Operations Differences from Original Design/Specification Basis

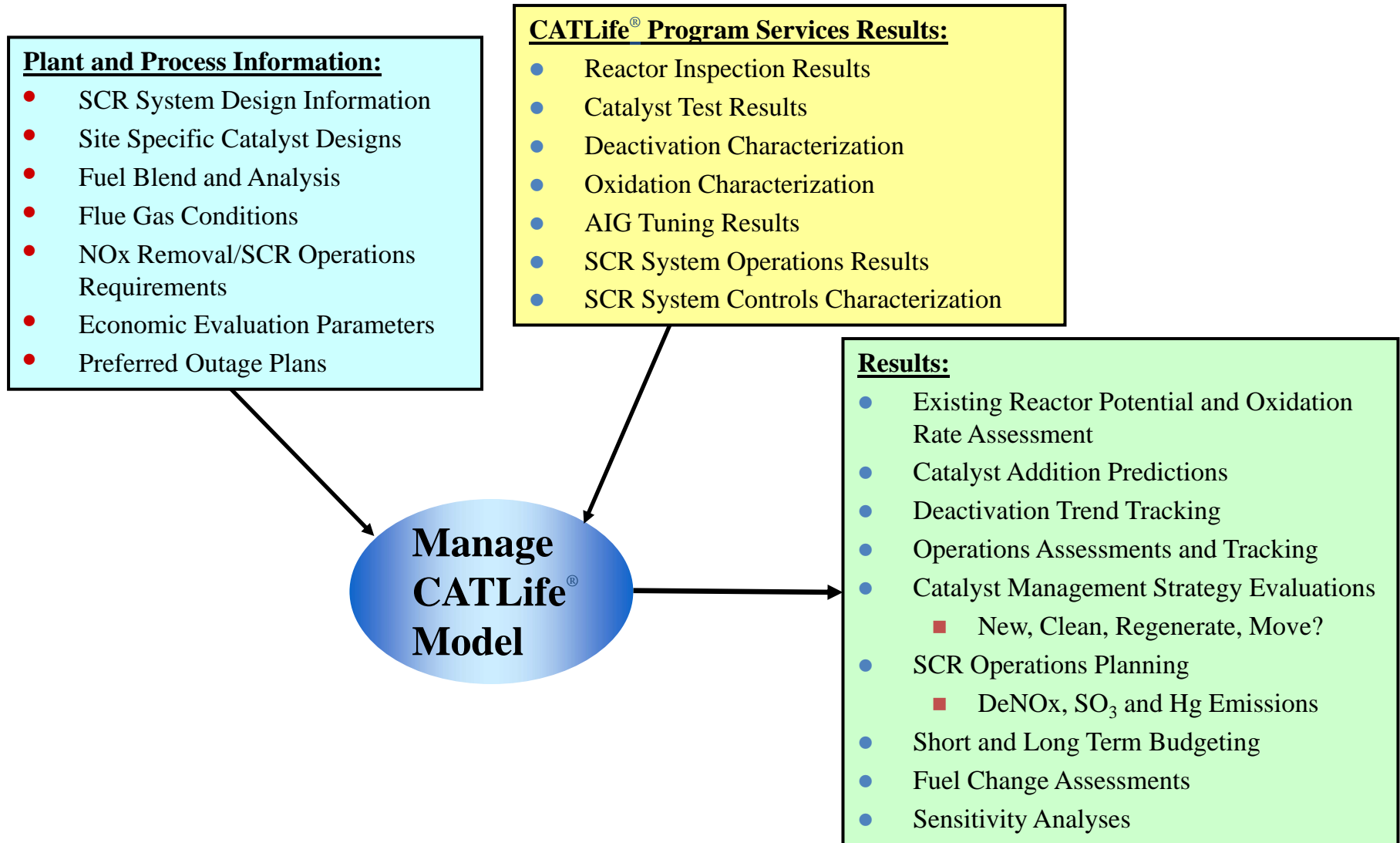


Catalyst Testing is Only One Part of Effective Catalyst Management

Activity	Objectives
AIG Checks and Tuning	Optimize NH ₃ /NO _x Distribution (Check/Tune Annually)
Monitor Ammonia in Ash	Test Frequently and Track Ammonia Slip Trends
Operations Data Assessment	Evaluate DeNO _x Demand (NO _x , T, Flow, Delta P, etc.)
Monitor Fuels Data	Evaluate Possible Effects on Catalyst
Reactor Inspections	Assess Pluggage and Mechanical Condition
Catalyst Testing	Assess Current Activity Levels and Deactivation Trends
Catalyst Management Planning	Evaluate Near Term SCR System Performance Capabilities
	Predict Next Need for Catalyst Addition
	Evaluate Options for Catalyst Addition (New vs Regen, etc.)

CERAM's Manage CATLife® Model Integrates All Considerations and Results to Assure Effective Catalyst Management Plan

CERAM's Manage CATLife® Model



CERAM's 20+ Years of SCR System and Catalyst Know How and Experience is Incorporated Into the Model

CERAM Working with King Plant

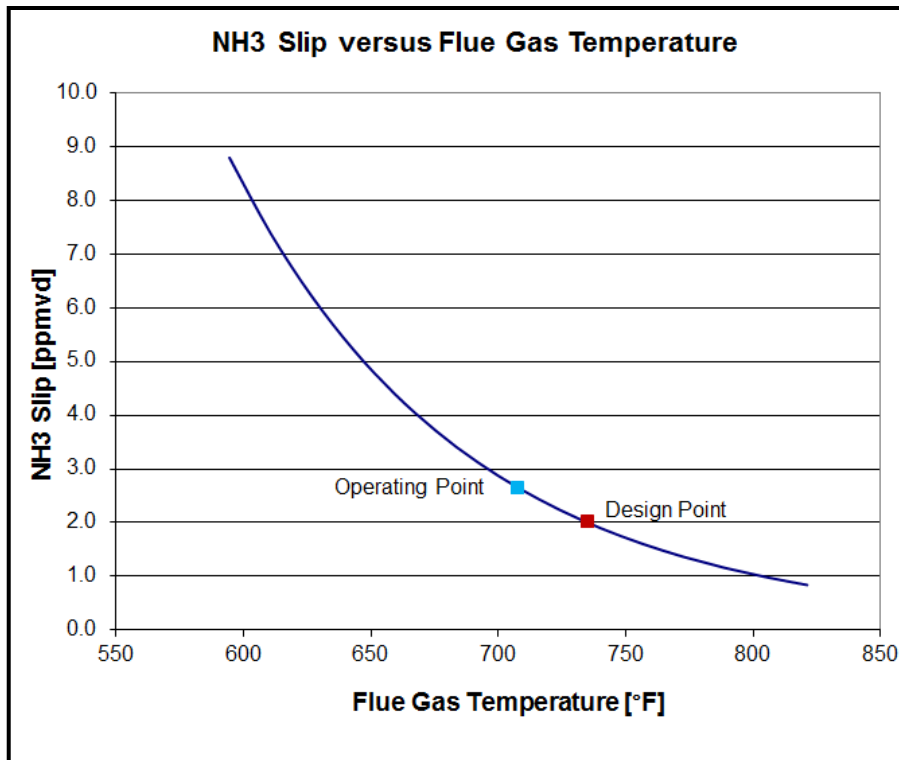
- **Develop Long Term Catalyst Management Plan to Fit Desired Outage Schedule**
 - **Replace One Layer Every 2 Years**
- Transition to Larger Catalyst Pitch
 - 8.2 mm CERAM replaced original 7.1 mm first layer in Spring 2011
 - 7.4 mm CERAM replaced original 7.1 mm second layer in Spring 2012
- Future 2 Year Replacement Cycle Achievable

King Plant

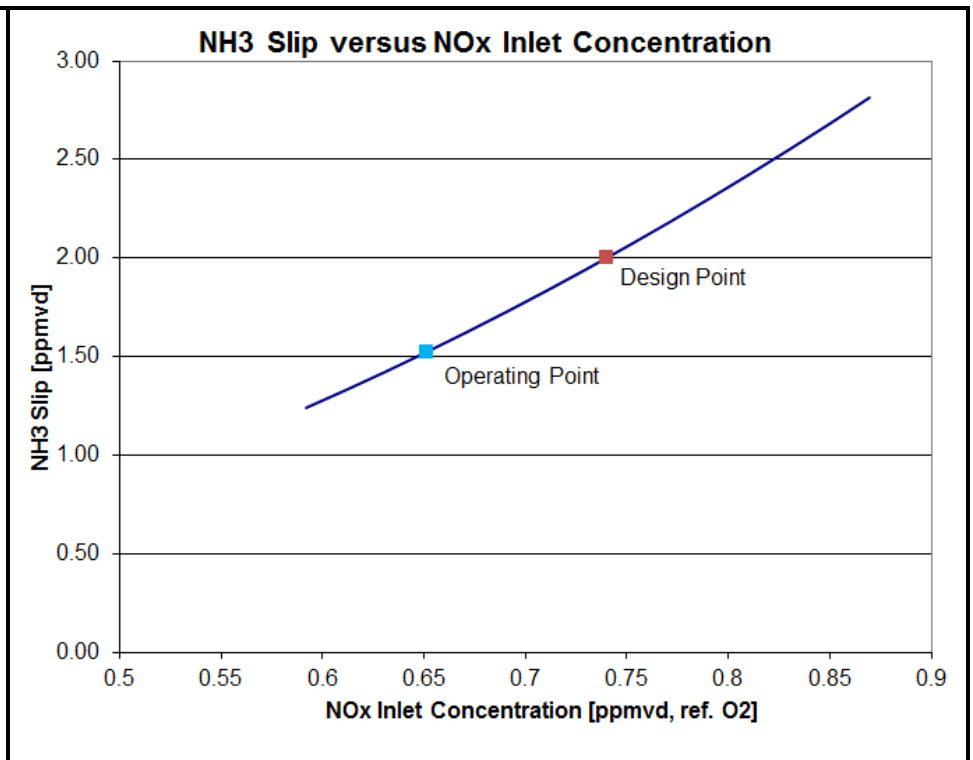
SCR Design Basis vs. Actual Operations

	Original Design Basis	2011 Operating Data Basis
Inlet NOx	0.74 lb/MBtu	0.65 lb/Mbtu
Outlet NOx	0.08 lb/Mbtu	0.08 lb/MBtu
Ammonia Slip	2.0 ppm	>2.0 ppm
Flue Gas Temperature	735° F	705° F
Catalyst Life	24,000	Future Catalyst Events Occur Every 2 Years

Effects of Temperature and Inlet NOx

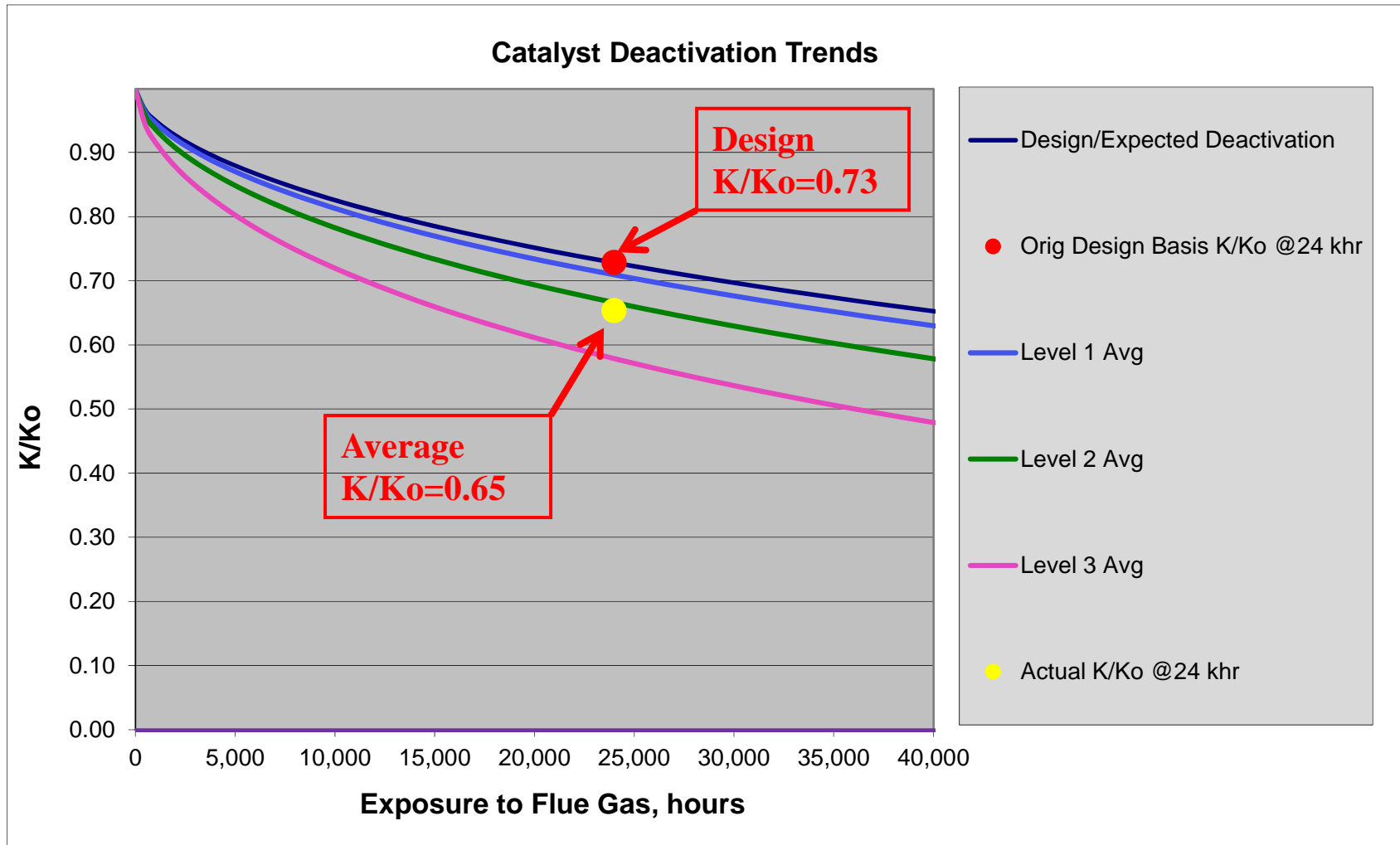


Reduced Temperature →
0.65 ppm NH₃ Slip Increase



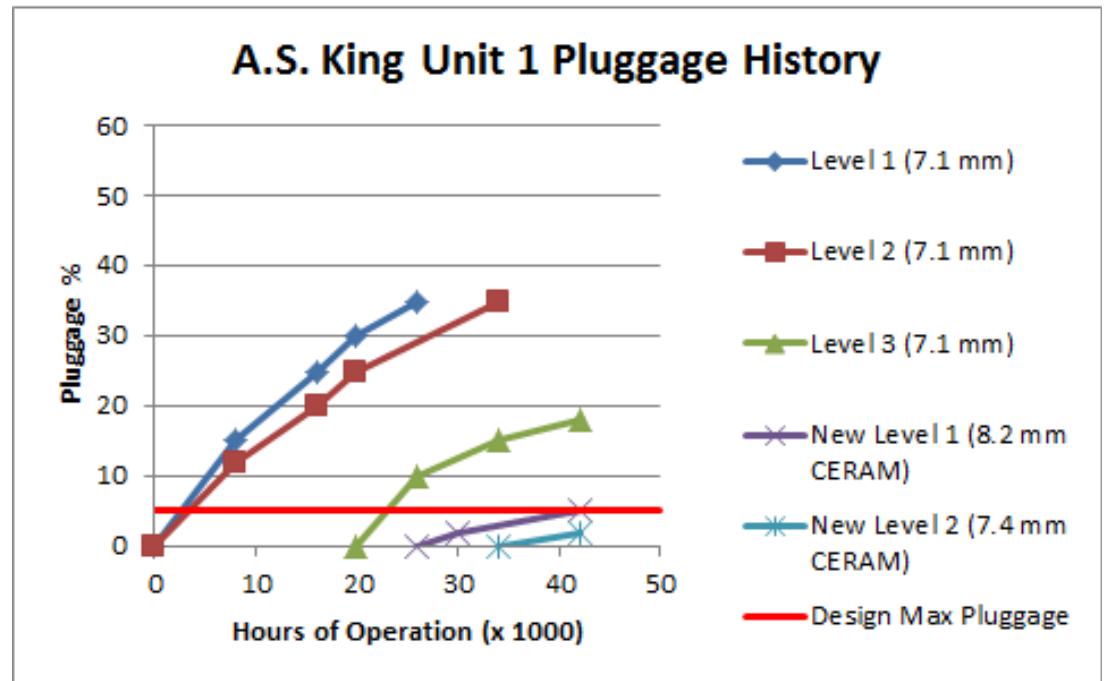
Reduced Inlet NOx →
0.48 ppm NH₃ Slip Decrease

King Plant Catalyst Deactivation Rate

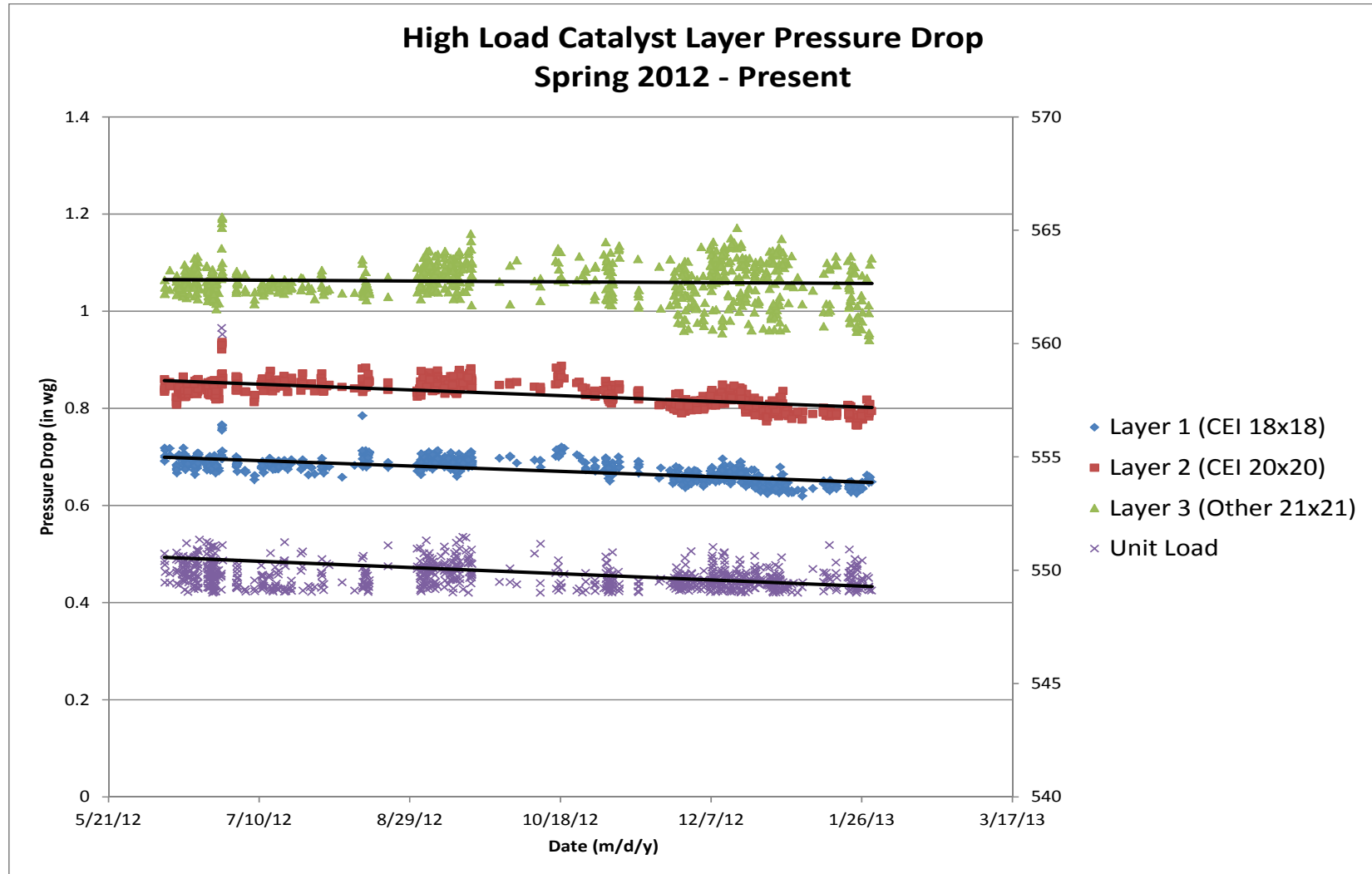


King Plant Catalyst Pluggage History

- 5% Design Pluggage
- 7.1 mm Pitch
 - >35% pluggage in 1st and 2nd levels
 - >15% pluggage in 3rd level
- 8.2 mm Pitch CERAM
 - Installed in 1st level Spring 2011
 - <5% pluggage after 2 years
- 7.4 mm Pitch CERAM
 - Installed in 2nd level Spring 2012
 - <5% pluggage after 1 year



Catalyst Pluggage Trends

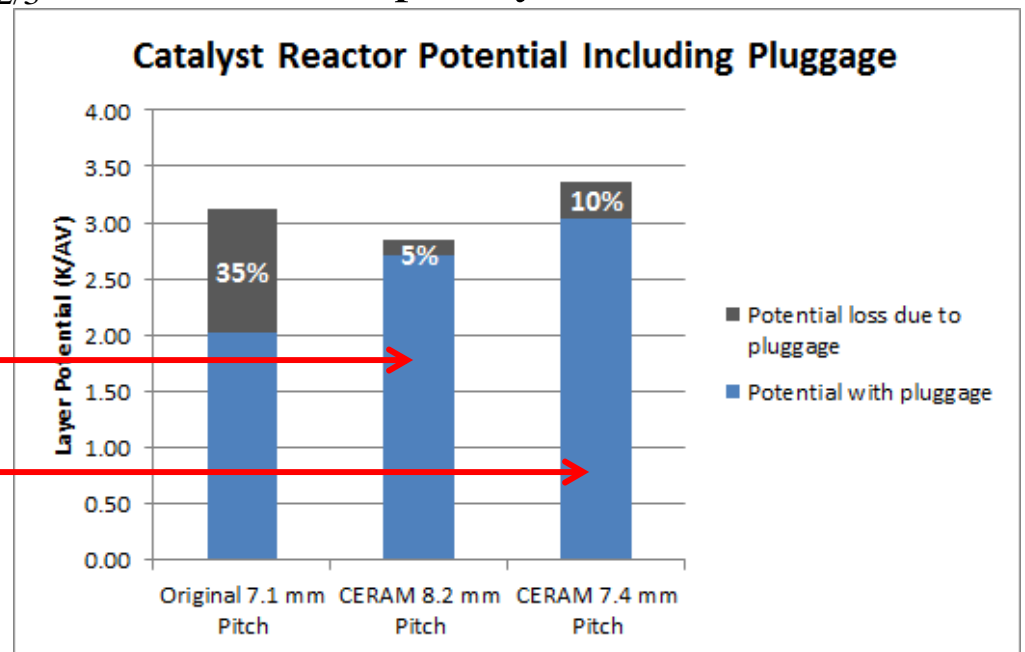


Proper Catalyst Selection – Geometry and Chemistry

- Catalyst Pitch Selection
 - We know 7.1 mm honeycomb is not the answer
 - Transitioning to larger pitch – reduced surface area must be offset by reduction in catalyst pluggage
 - 8.2 mm pitch has 16% less specific surface area compared to 7.1 mm
 - 7.4 mm pitch has 7% less specific surface area compared to 7.1 mm
- Catalyst Chemistry Selection
 - Existing catalyst is 0.5% $\text{SO}_{2/3}$ conversion rate per layer
 - Increasing the $\text{SO}_{2/3}$ conversion to 1.0% per layer will increase activity by approximately 10%

34% More Potential

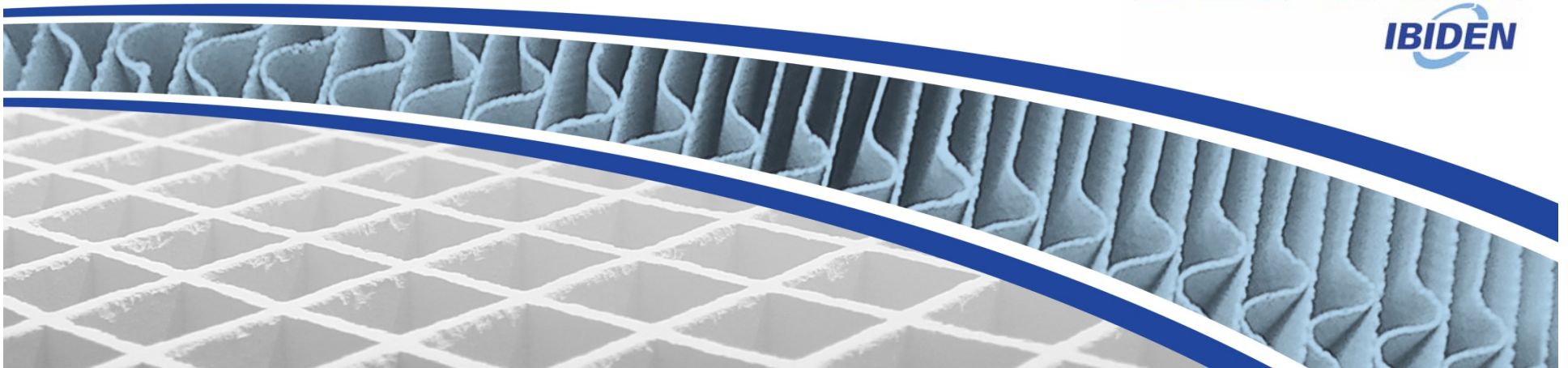
49% More Potential



A.S. King Unit 1

Catalyst Management Plan Comparison

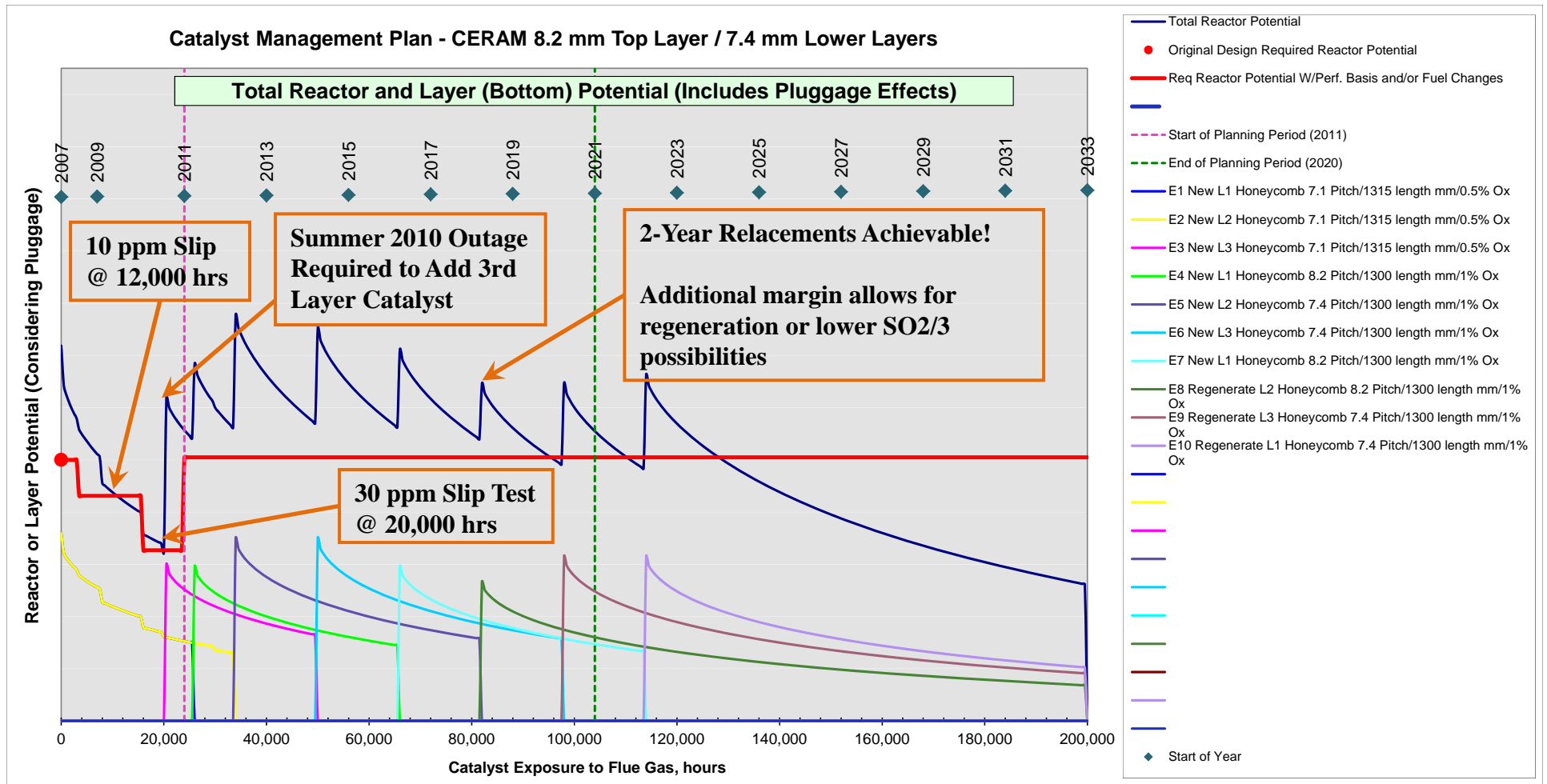
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CERAM Working with King Plant

- **Develop Long Term Catalyst Management Plan to Fit Desired Outage Schedule**
 - **Replace One Layer Every 2 Years**
- Transition to Larger Catalyst Pitch
 - 8.2 mm CERAM replaced original 7.1 mm first layer in Spring 2011
 - 7.4 mm CERAM replaced original 7.1 mm second layer in Spring 2012
- Future 2 Year Replacement Cycle Achievable

Current CMP with Recommended Changes



10 Year CMP Economics (2011-2020)

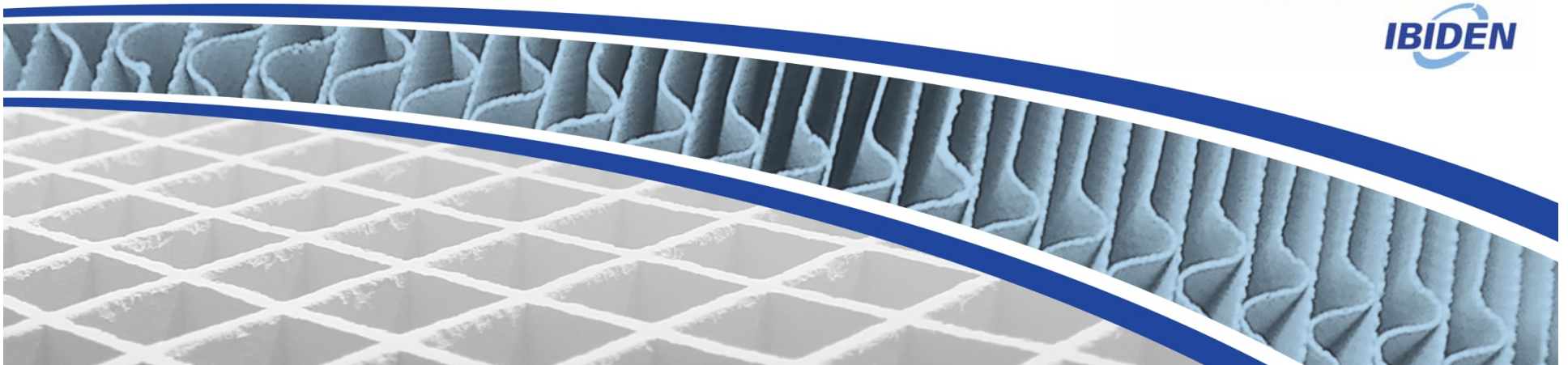
Net Present Value Analysis in 2013 Dollars			
	Status Quo	CERAM CMP	Differential
Number of Catalyst Events (2011 to 2020)	8	6	2 Fewer Events
Catalyst Related Expenditures	\$ 13,235,000	\$ 9,944,000	\$ 3,291,000
Fan Energy Costs for Reactor Pressure Drop	\$ 3,377,000	\$ 2,352,000	\$ 1,025,000
DeNOx System Ammonia Cost	\$ 16,479,000	\$ 16,479,000	\$ 0
Total Net Present Value of Plan (2011 to 2020)	\$ 33,091,000	\$ 28,775,000	\$ 4,316,000
NPV NOx Removal Cost of Plan (2011 to 2020)	298 \$/ton	259 \$/ton	39 \$/ton

Note: Economics do not consider replacement power costs associated with untimely outages!

2013 Reinhold Presentation

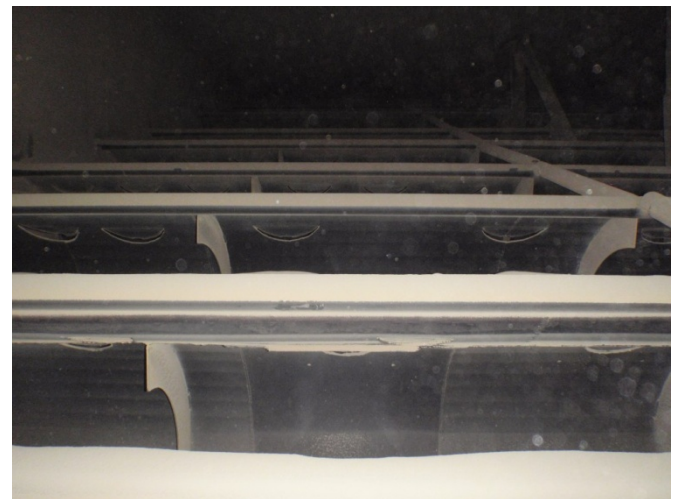
NIPSCO Bailly Unit 8 “Trials and Tribulations”

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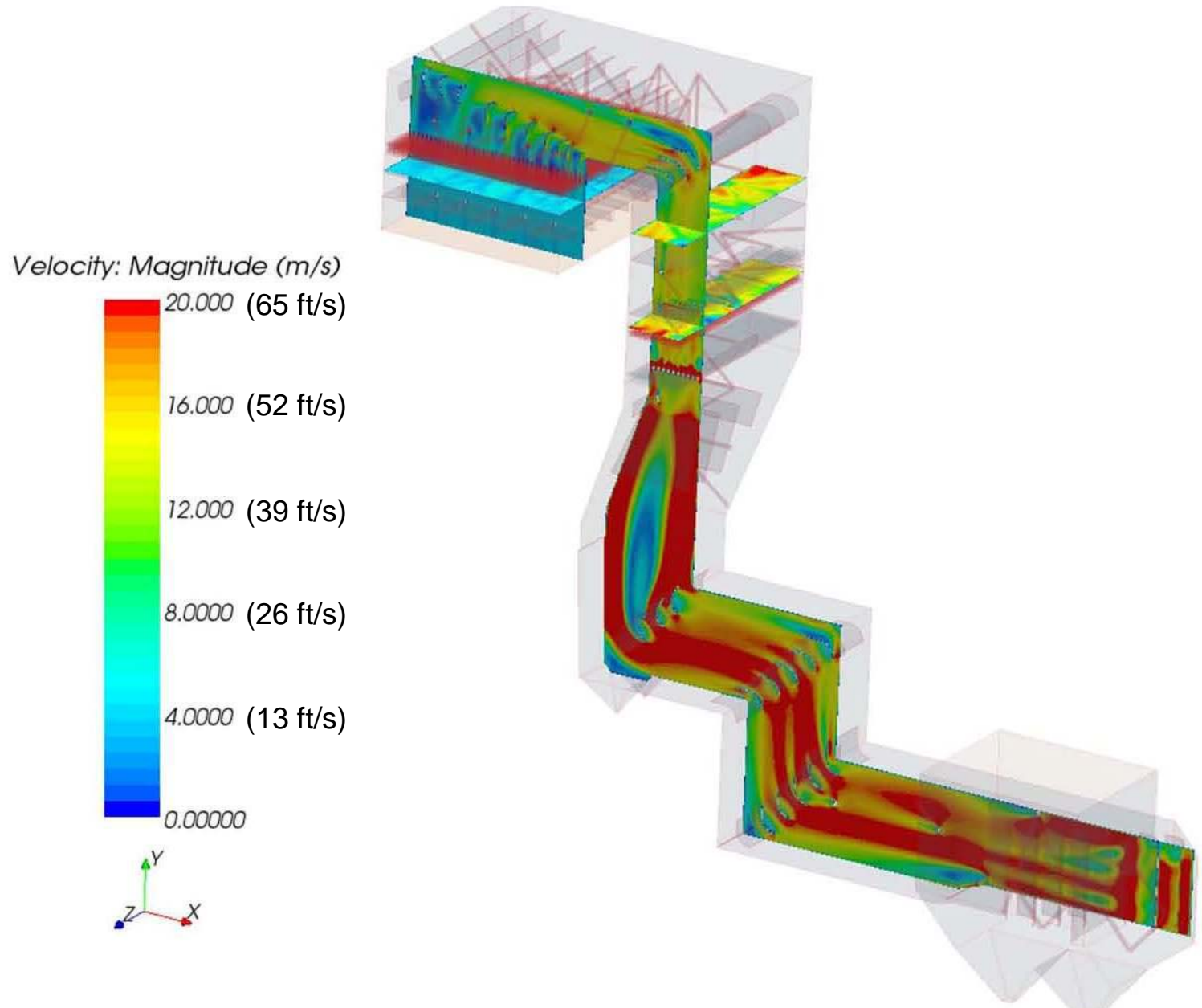


Bailly Unit 8 Overview

- 360 MWg
- B&W Cyclone Boiler (3,400 MMBtu/hr)
- Eastern Bituminous Coal Fired
 - Sulfur \approx 2.5-3.5%
 - Ash \approx 9-10%
- SCR in Service 2004
 - 3 + 1 Reactor
 - 12 x 7 Module Arrangement Per Layer
 - CERAM Honeycomb 6.7 mm Pitch Catalyst
 - Fuel Tech NOxOut Ultra System
- Originally Sootblowers Installed L1 & Sonic Horns Installed L2 & L3
- Physical Flow Model Demonstrated All Distributions Achieved and No Ash Drop Out



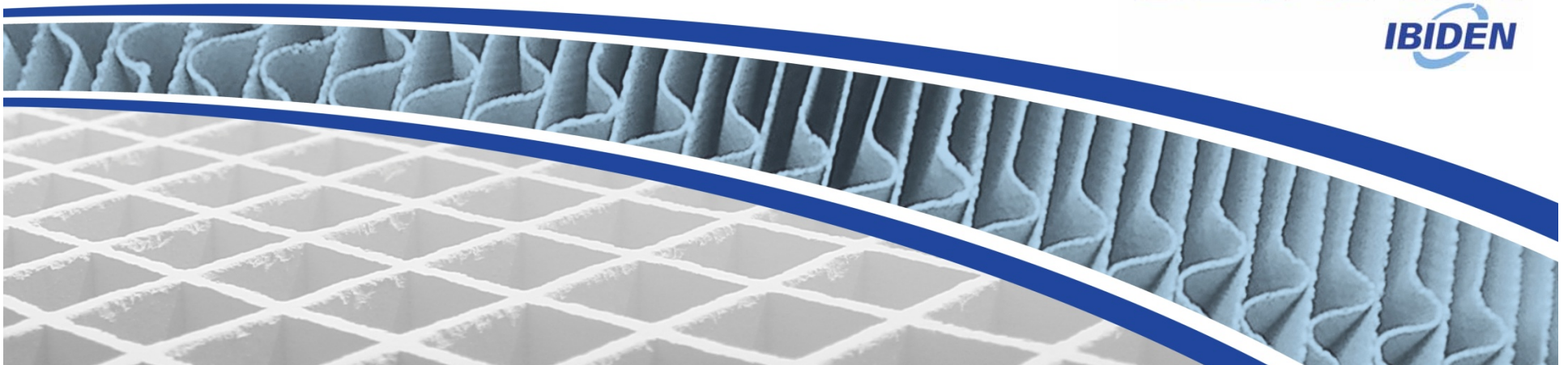
Bailly Unit 8 Schematic



2013 Reinhold Presentation

NIPSCO Bailly Unit 8 Reactor Inspection Review

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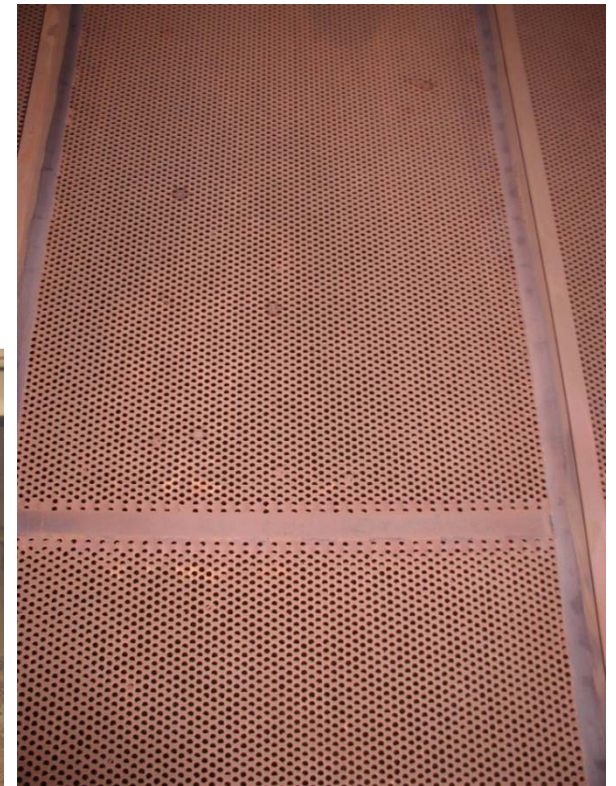


Bailly Unit 8 Reactor Inspection Overview

- Annual Reactor Inspection Performed Over Past 8 Years
 - Frame by Frame Assessment of Pluggage
 - Inspect Catalyst Baffle Plates/Seals, Ammonia Injection Grid (AIG), Large Particle Ash (LPA) Screen, Flow Correction Devices (Guide Vanes, Mixers, etc.), Accessible Duct Work (e.g., Crossover Duct, Inlet Duct, etc.)
 - Historically Pluggage Observed Due to LPA, Unburned Carbon and Ash Dropout (Velocity Maldistribution?)
 - Ash Piles (3-8 ft) Observed In L1, L2 & L3 (East Side)
 - Severe Pluggage Across East & South/Southeast Side Of Reactor
 - At Times Module Pluggage 5-100% in L1, L2 & L3
 - Catalyst Management Ensured Target Emissions Always Achieved
 - Solutions Developed and Implemented to Eliminate Pluggage
 - Ash Buildup On North Section of AIG Lances; Nozzle Pluggage
 - Vanes 2 & 3 In Reactor Hood Missing Flow (e.g., Appear “Dirty”)

Bailly Unit 8 Reactor Inspection Overview

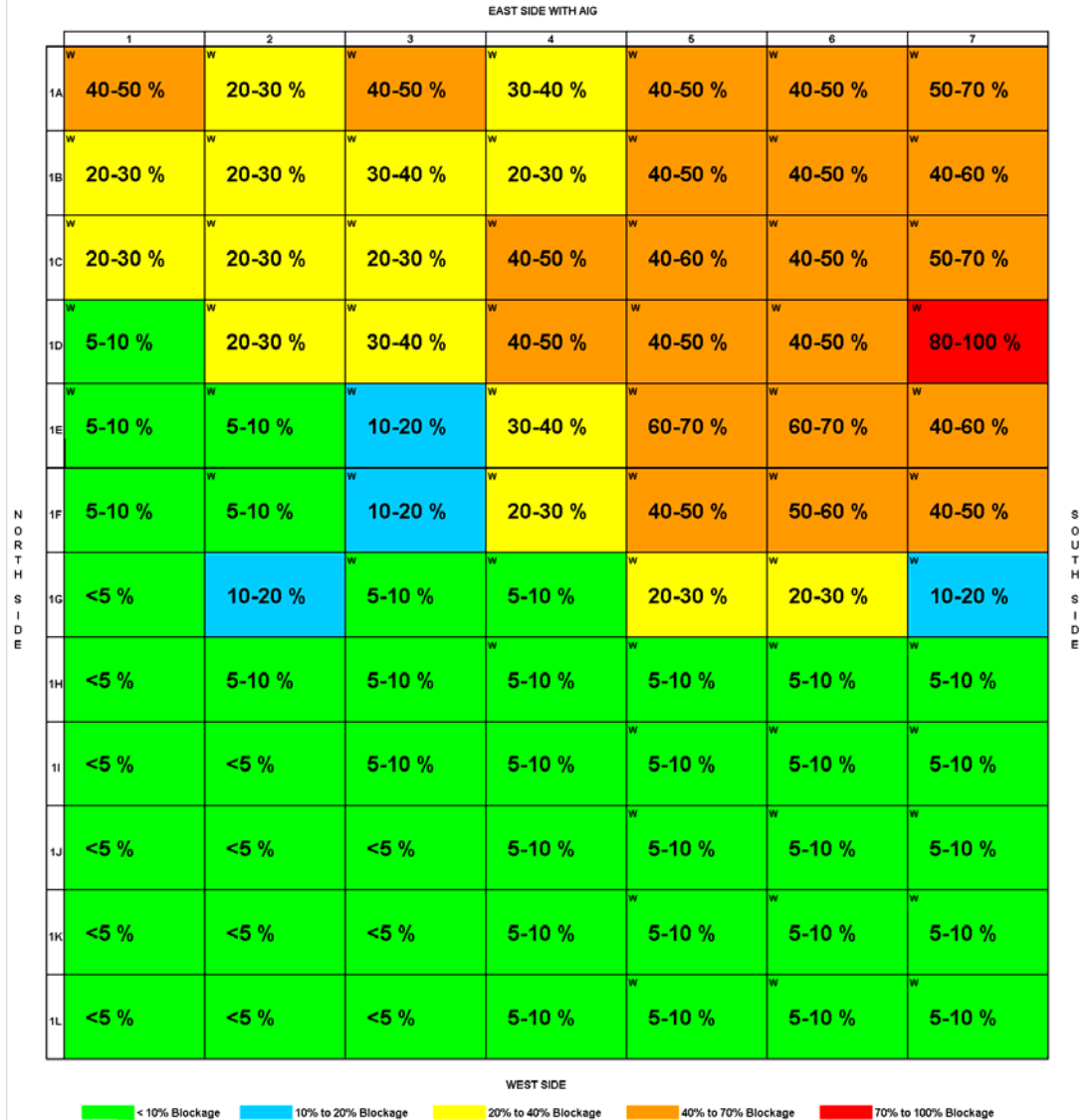
- LPA (Popcorn Ash) Attributed to Plugging
- Original LPA Screen Design
 - 50% Open Perforated Plate (1/2" Diameter Holes)
 - Installed At Non-Inverted Angle Above Economizer Outlet Hoppers
 - Significant Quantities of LPA Deposited On/In Catalyst
 - Recommended Alternative Design



Bailly Unit 8 Reactor Inspection Overview



Top Catalyst Layer for Bailly Unit 8
 "Clean" Reactor Inspection
 October 19, 2005



Note: Reference "Dirty" inspection diagram for locations of Unburned Carbon, Popcorn Ash / LPA and Fly Ash Piles.

Bailly Unit 8 Reactor Inspection Overview

Middle Catalyst Layer for Bailly Unit 8
 "Clean" Reactor Inspection
 October 19, 2005

EAST SIDE WITH AIG

	1	2	3	4	5	6	7
2A	30-40%	40-50%	40-50%	15-20%	15-20%	20-30%	20-30%
2B	20-30%	30-40%	20-40%	50-60%	20-30%	20-30%	20-40%
2C	20-30%	20-30%	20-30%	30-40%	10-20%	20-30%	20-30%
2D	5-10%	10-20%	10-20%	40-50%	40-50%	80-100%	80-100%
2E	10-20%	10-20%	20-40%	10-20%	40-50%	20-30%	20-30%
2F	5-10%	5-10%	5-10%	10-20%	40-50%	30-40%	20-40%
2G	<5%	<5%	10-15%	20-30%	10-20%	10-20%	10-20%
2H	<5%	<5%	5-10%	10-20%	15-20%	10-20%	10-20%
2I	<5%	<5%	<5%	10-20%	10-20%	10-20%	10-20%
2J	<5%	<5%	<5%	5-10%	10-20%	10-20%	10-20%
2K	<5%	<5%	<5%	5-10%	10-20%	10-20%	10-20%
2L	<5%	<5%	<5%	5-10%	10-20%	10-20%	10-20%

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WEST SIDE

■ < 10% Blockage
 ■ 10% to 20% Blockage
 ■ 20% to 40% Blockage
 ■ 40% to 70% Blockage
 ■ 70% to 100% Blockage

W = Washed in March 2005

Note: Reference "Dirty" Inspection diagram for locations of Unburned Carbon, Popcorn Ash / LPA and Fly Ash Piles.

Bailly Unit 8 Reactor Inspection Overview

- Replaced Perforated LPA Screen with STEAG LPA Screen
 - Significantly Less LPA Observed After New LPA Screen
 - Eliminate LPA From Reactor?
 - Design Allowed “Cleaning” by Pulling Chain To Move Screen
 - Release Screen; Strike Stoppers; Force Drops LPA To Hoppers
 - Seal Installation Around Screen Resulted In LPA Present In Reactor
 - “Fixed” Position of LPA Screen (Does Not Move)
 - Eliminated LPA From Reactor

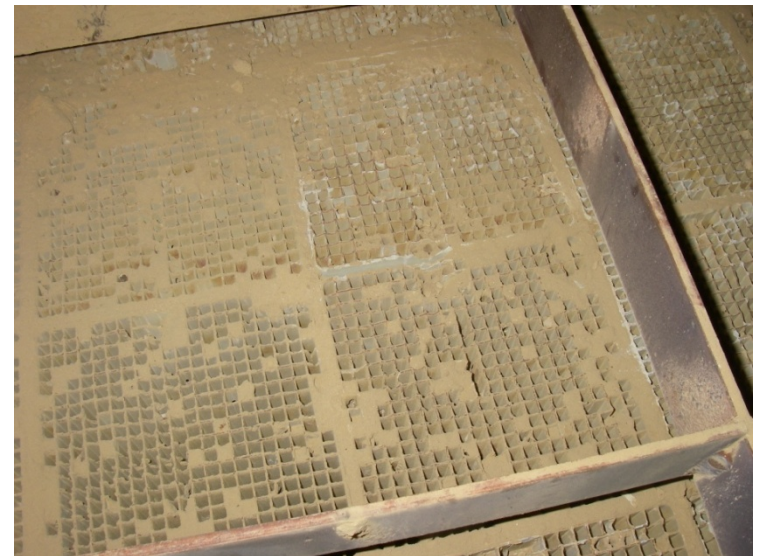


Bailly Unit 8 Reactor Inspection Overview

- High Levels of Unburned Carbon Typically Observed In Reactor
 - Contributed to Pluggage and Localized Sintering
 - Recommended To Reduce LOI Levels to $<15\%$ Measured Upstream of Reactor



Example of “Mechanical” Cleaning Not Recommended



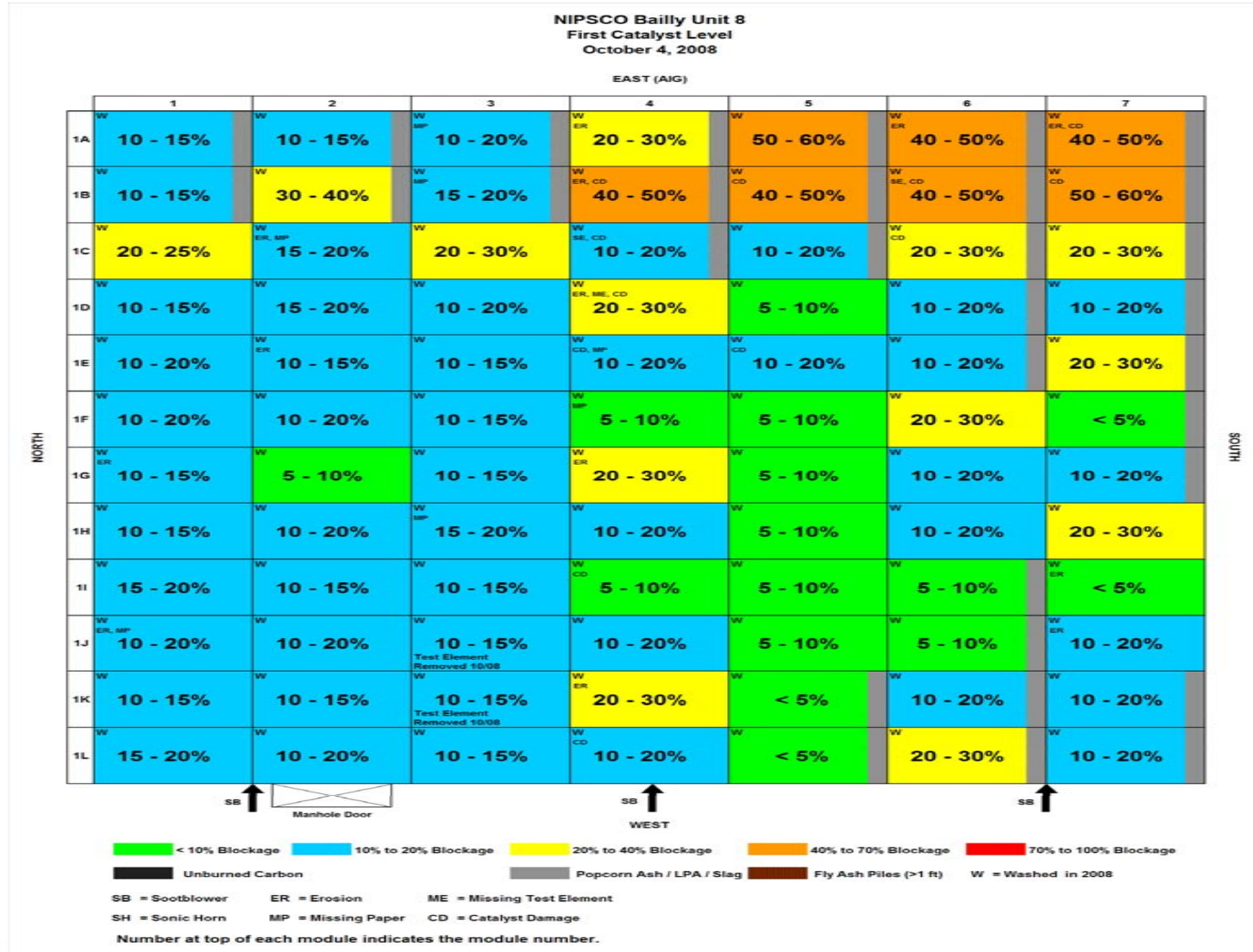
Discontinued by NIPSCO

Bailly Unit 8 Reactor Inspection Overview

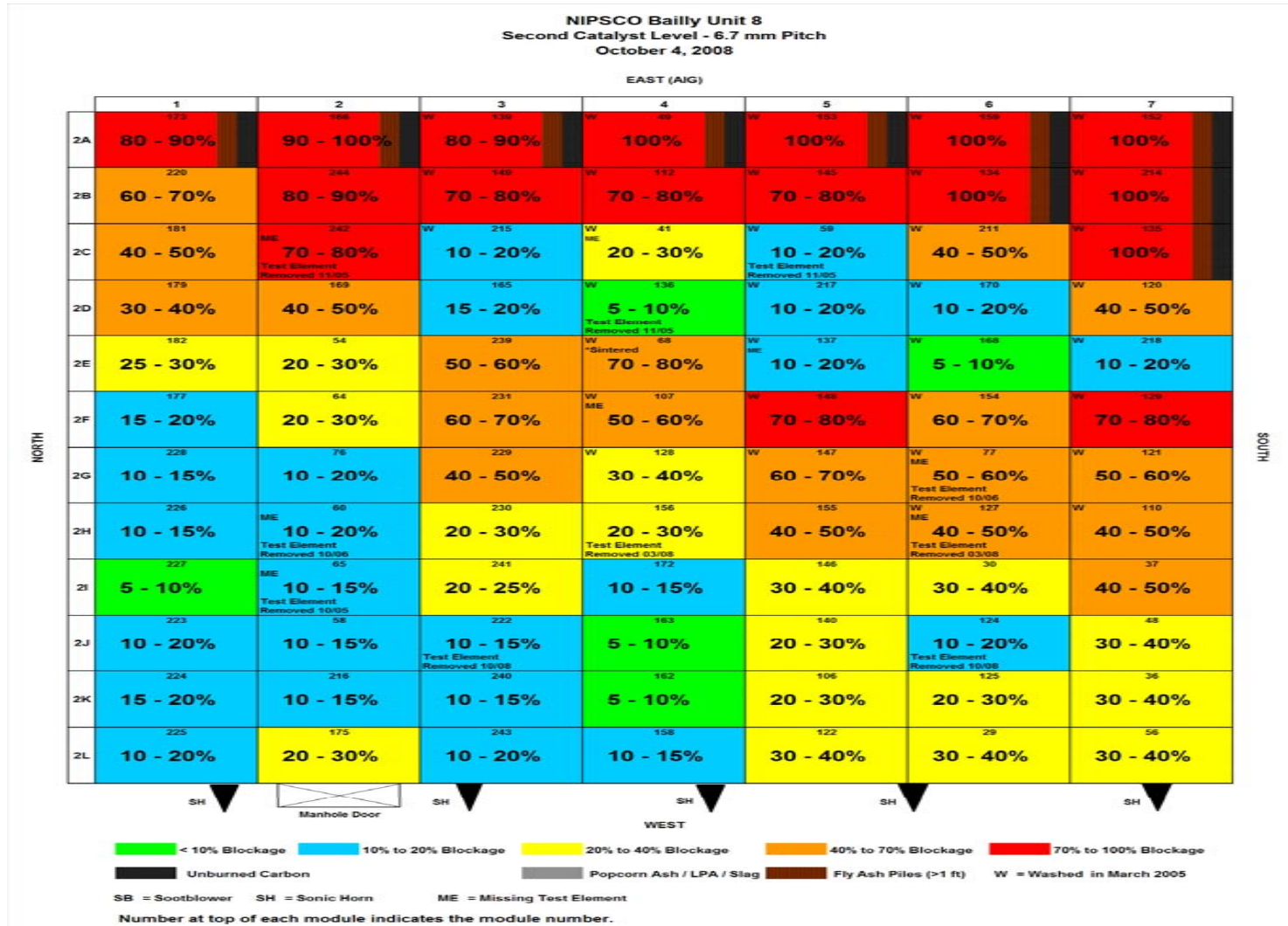
- Ash Dropout In Reactor Severe Along East Side & Southeast Corner
- Ash Piles 3-8 ft Observed (Modules 80-100% Plugged)
- “Normal” Pluggage L1 = 18% (L1 Washed; was 64%), L2 pluggage = 40%, L3 pluggage = 35%



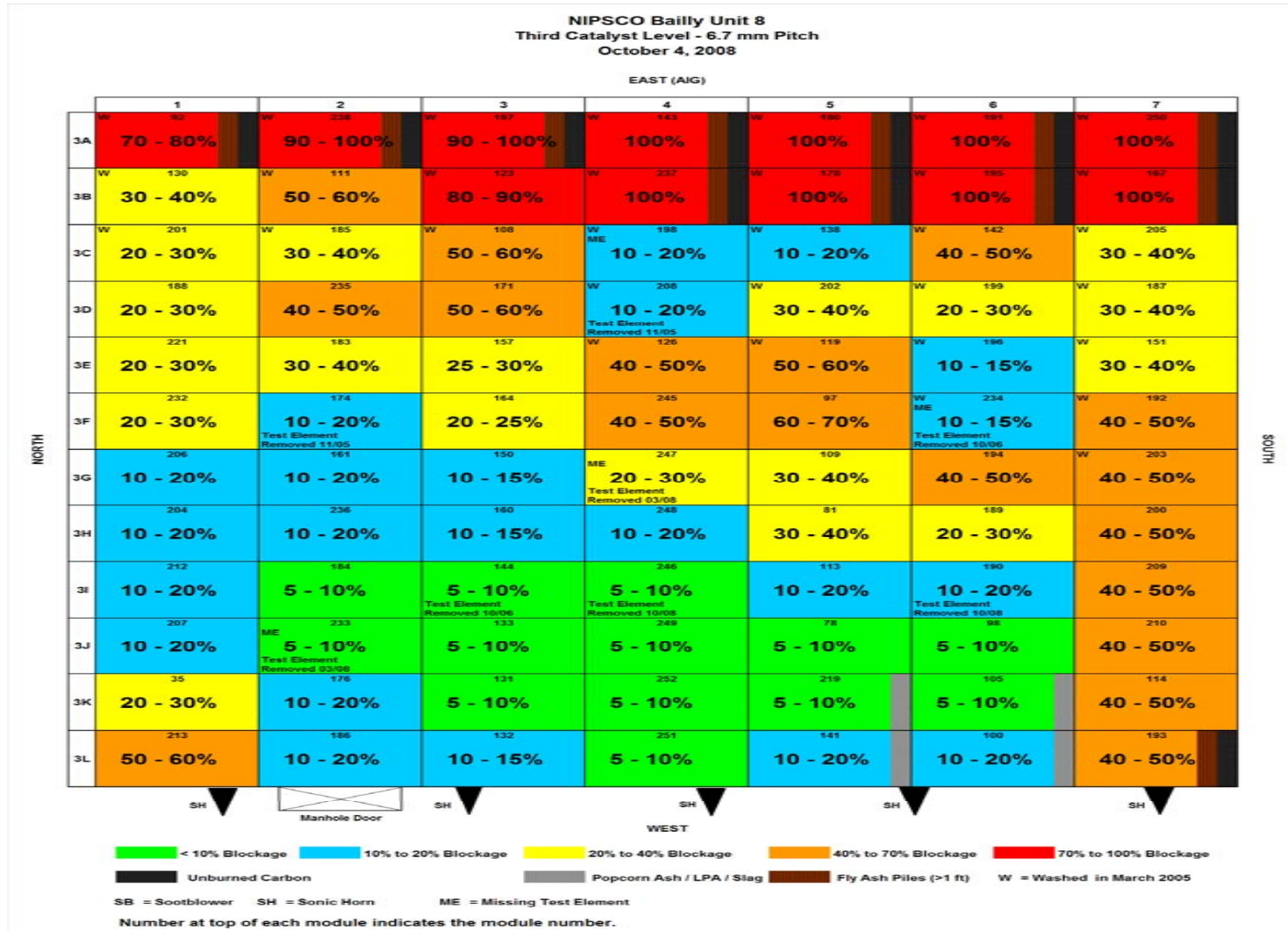
Bailly Unit 8 Reactor Inspection Overview



Bailly Unit 8 Reactor Inspection Overview



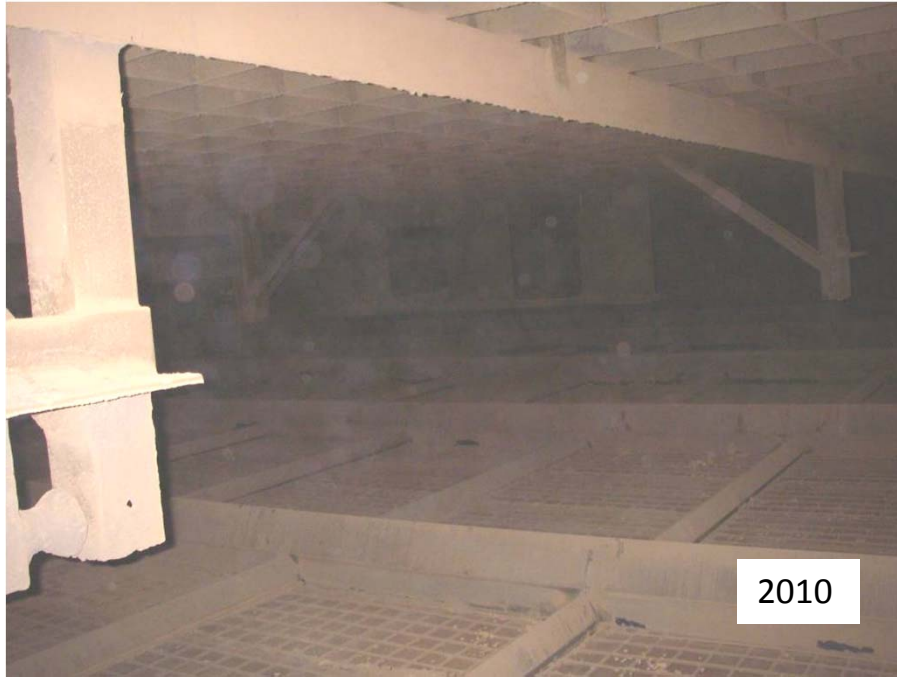
Bailly Unit 8 Reactor Inspection Overview



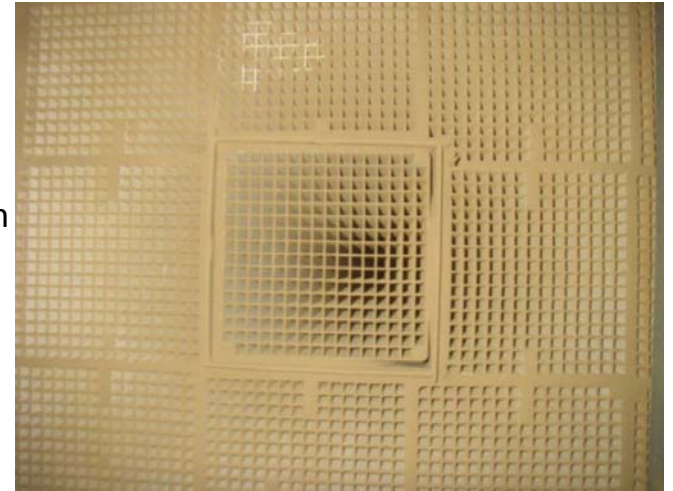
Bailly Unit 8 Reactor Inspection Overview

- Recommended CFD Modeling From Economizer Outlet to SCR Outlet
 - Original Flow Model Did Not Include CFD (Not Performed by Fuel Tech)
 - Physical Test Results Aided in Guide Vane Design & Location (Circa 2002-03)
 - Assumed Plug Flow From Economizer; $\pm 15\%$ Vel. Distribution
 - Reactor Internals Available Modeled (Gussets Perpendicular To Flow, etc.)
 - Height From Crossover Duct To Top of Catalyst In Level 1 Approx. 6 ft (Swirls & Eddies Present Based on Inspections)
 - Vanes 2 & 3 In Reactor Hood Missing Flow (e.g., Appear “Dirty”)
 - Ash Buildup on North Section of AIG Lances; South Side Clean; Southeast Side of Reactor Had Highest Pluggage
- 2009 L1 Replaced With 9.2 mm Pitch To Act As Catalyst/Flow Rectifier “Band-Aid” Until CFD Model
 - Piles On Lower Levels Not As Severe But Present
 - Best-of-Best Made in Lower Levels
 - 2008-09 Sonic Horns Installed L1; Sootblower Pipes Removed

Bailly Unit 8 Reactor Inspection Overview



9.2 mm Pitch
Level 1



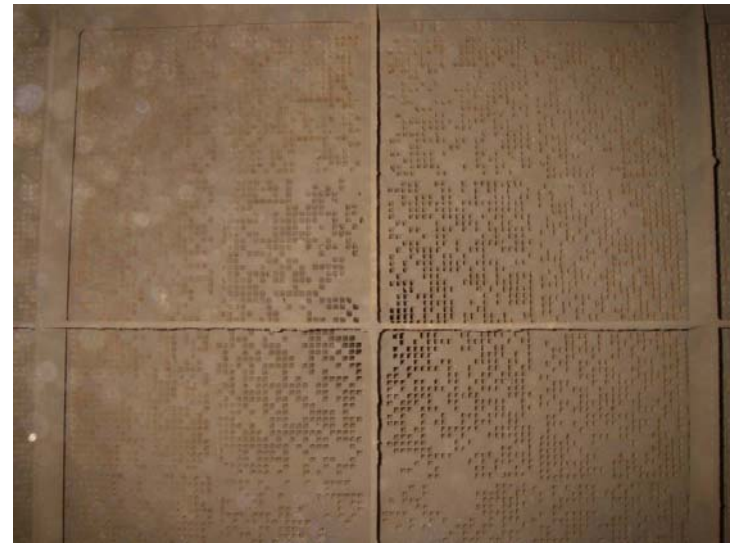
Avg pluggage:
L1 = 5% (9.2 mm),
L2 = 35% (6.7 mm),
L3 pluggage = 25% (6.7 mm)
(End of 2009; L1 (18%), L2 (40%) & L3 (35%))



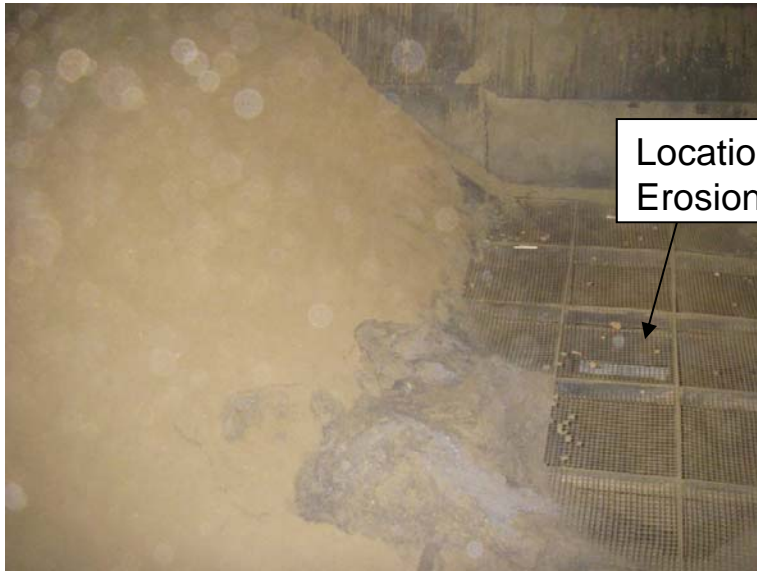
Bailly Unit 8 Reactor Inspection Overview



Level 2
6.7 mm Pitch



Bailly Unit 8 Reactor Inspection Overview



Level 2

Location of
Erosion (2010)



Bailly Unit 8 Reactor Inspection Overview



Seal damage (material type)



IBIDEN Mechanical cleaning and erosion



Bailly Unit 8 Reactor Inspection Overview



AIG

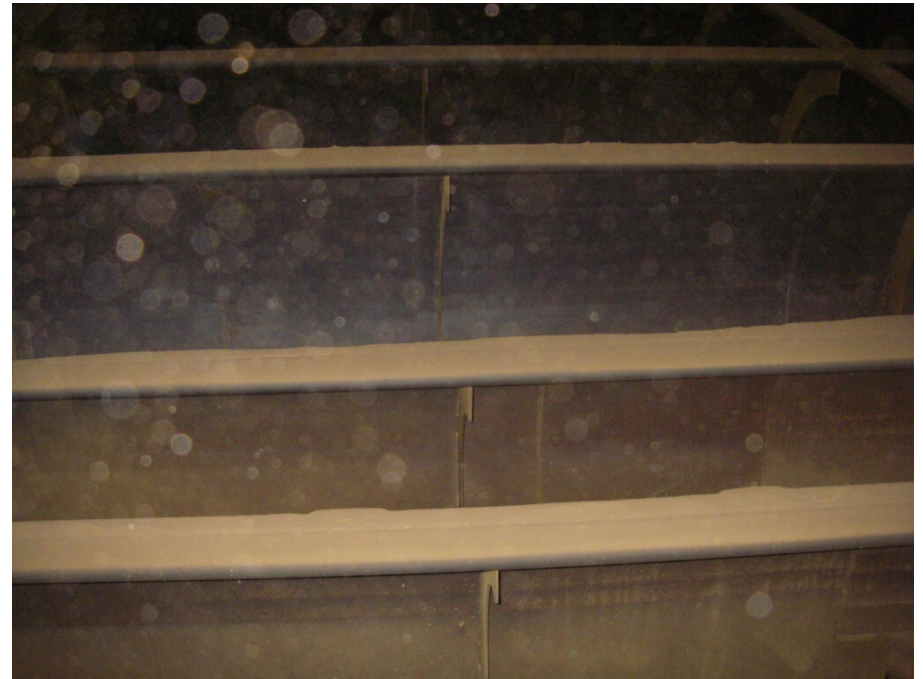
Valves all insulated



Bailly Unit 8 Inspection Results Overview



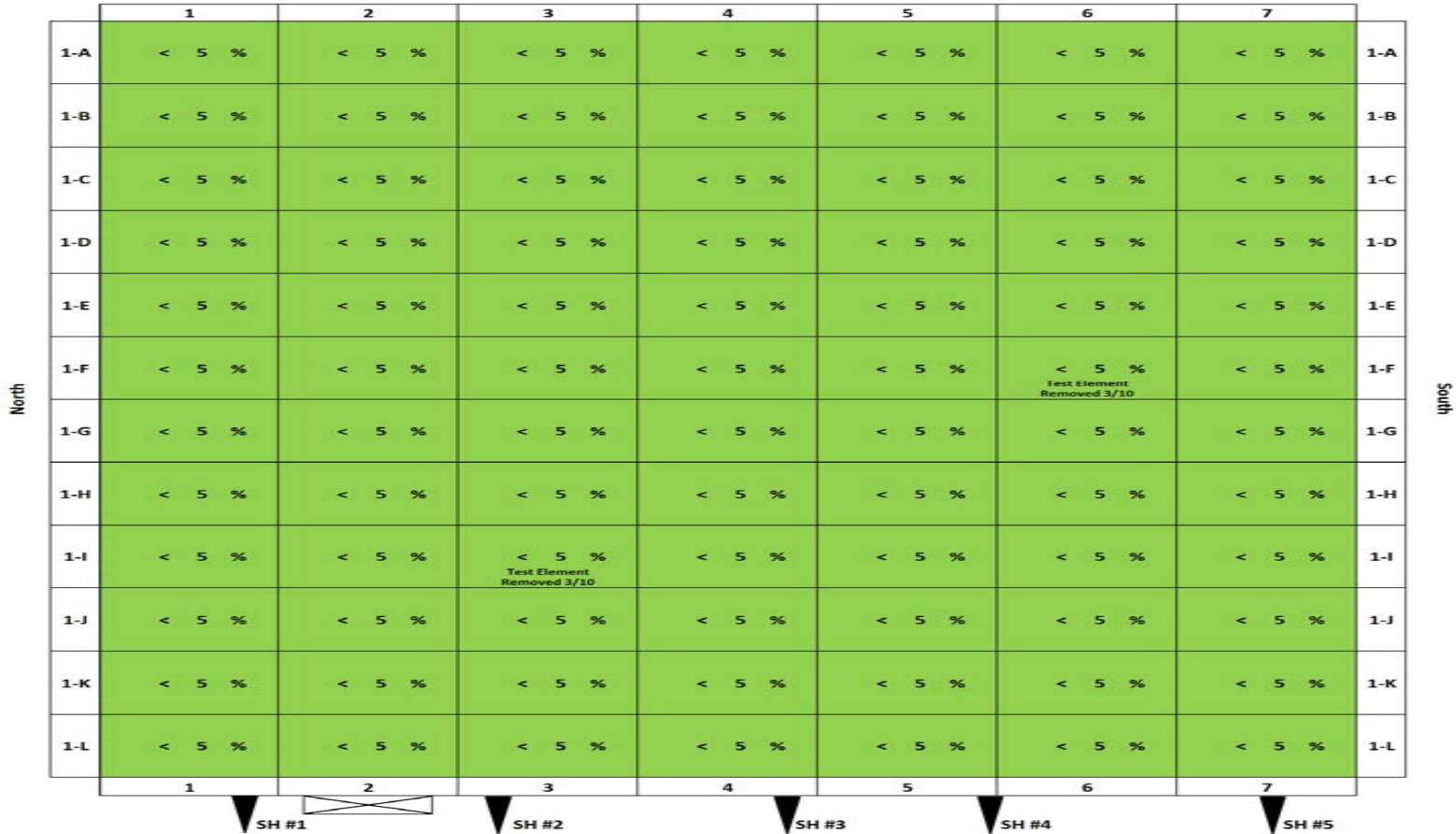
“Clean” vs. “Dirty” Vanes



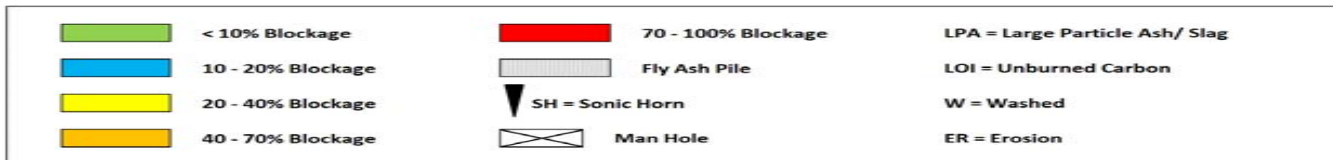
Scallops Used

**Bally Unit 8
Pluggage Diagram
First Catalyst Level (9.2 mm Pitch)
March 3, 2010**

East Side (AIG)

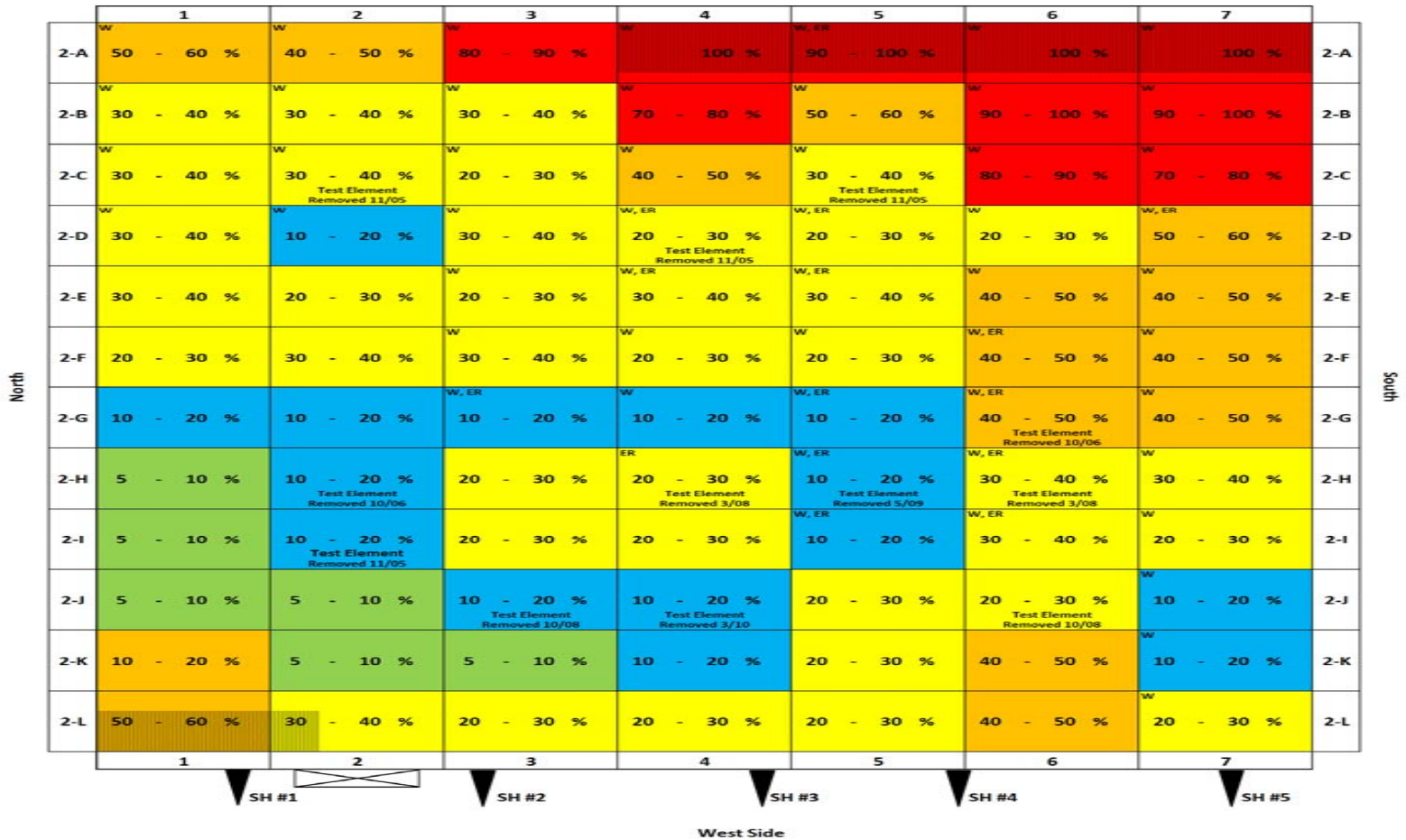


West Side



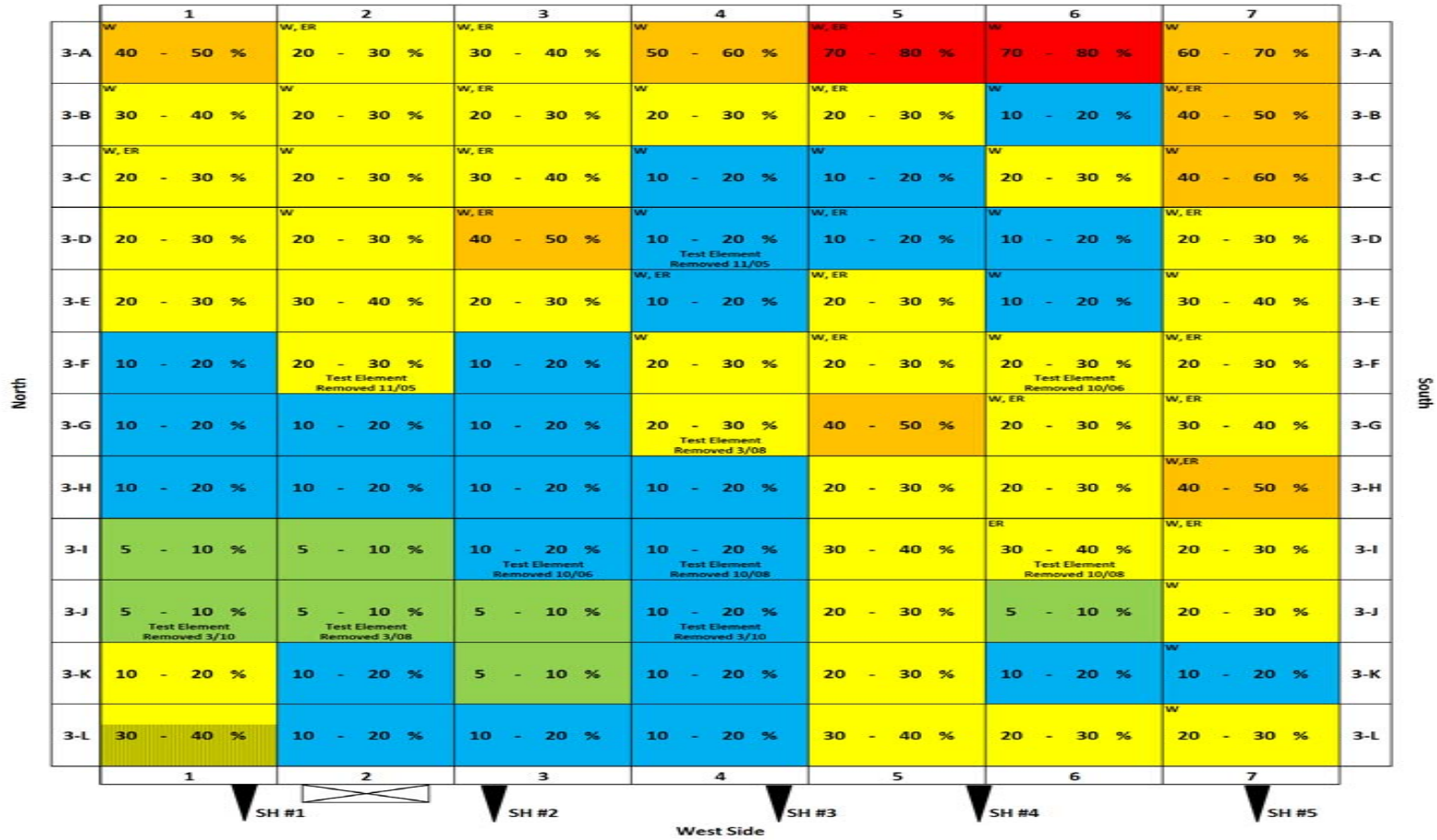
Bailly Unit 8
Pluggage Diagram
Second Catalyst Level (6.7 mm Pitch)
March 3, 2010

East Side (AIG)



Bailly Unit 8
Pluggage Diagram
Third Catalyst Level (6.7 mm Pitch)
March 3, 2010

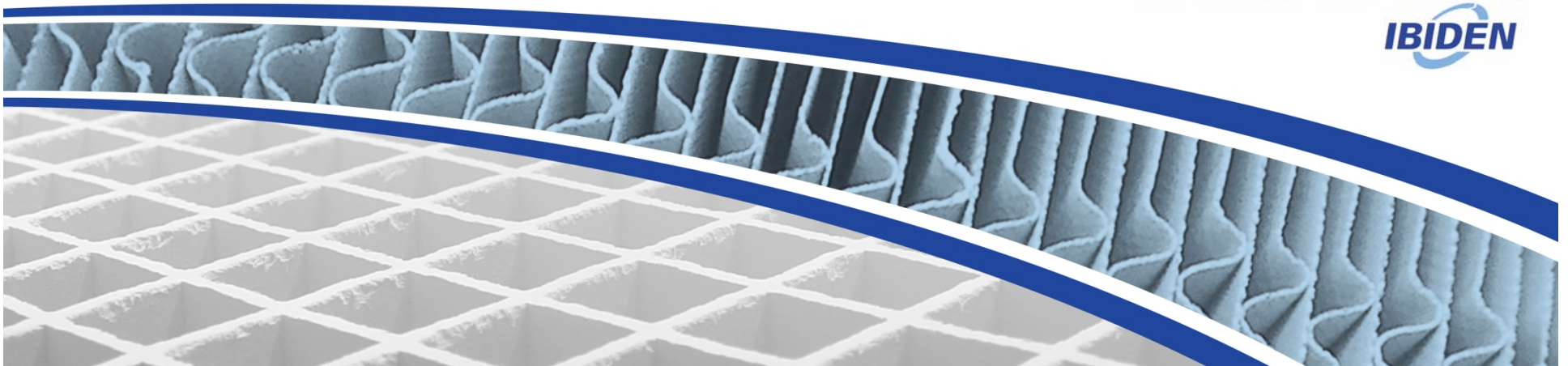
East Side (AIG)



2013 Reinhold Presentation

NIPSCO Bailly Unit 8 CFD Modeling & Modifications

CERAM
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Bailly Unit 8 CFD Modeling Study – Goal of Study to Improve Flow Distribution

- CFD Modeling Performed by Fuel Tech, Inc.
- CFD Baseline Demonstrated High Velocity Distribution (Approx 43%)
 - Flue Gas Distribution Upstream of AIG = 100% of points within 15% of the mean
 - Flue Gas Distribution Upstream of Catalyst = 100% of points within 15% of the mean

Summary	% with in 10 %	% with in 15	RMSE
Run			
Baseline (existing configuration)	15.3	23.9	43.5

- Examine “Finger-Vanes” in Vertical Riser Duct; Ash Buildup On North Side of AIG; No Ash Buildup On South Side of AIG
- Dirty vs. Clean Vanes in Reactor Hood
- Ash Dropout East and Southeast Side of Reactor



Velocity: Magnitude (ft/s)

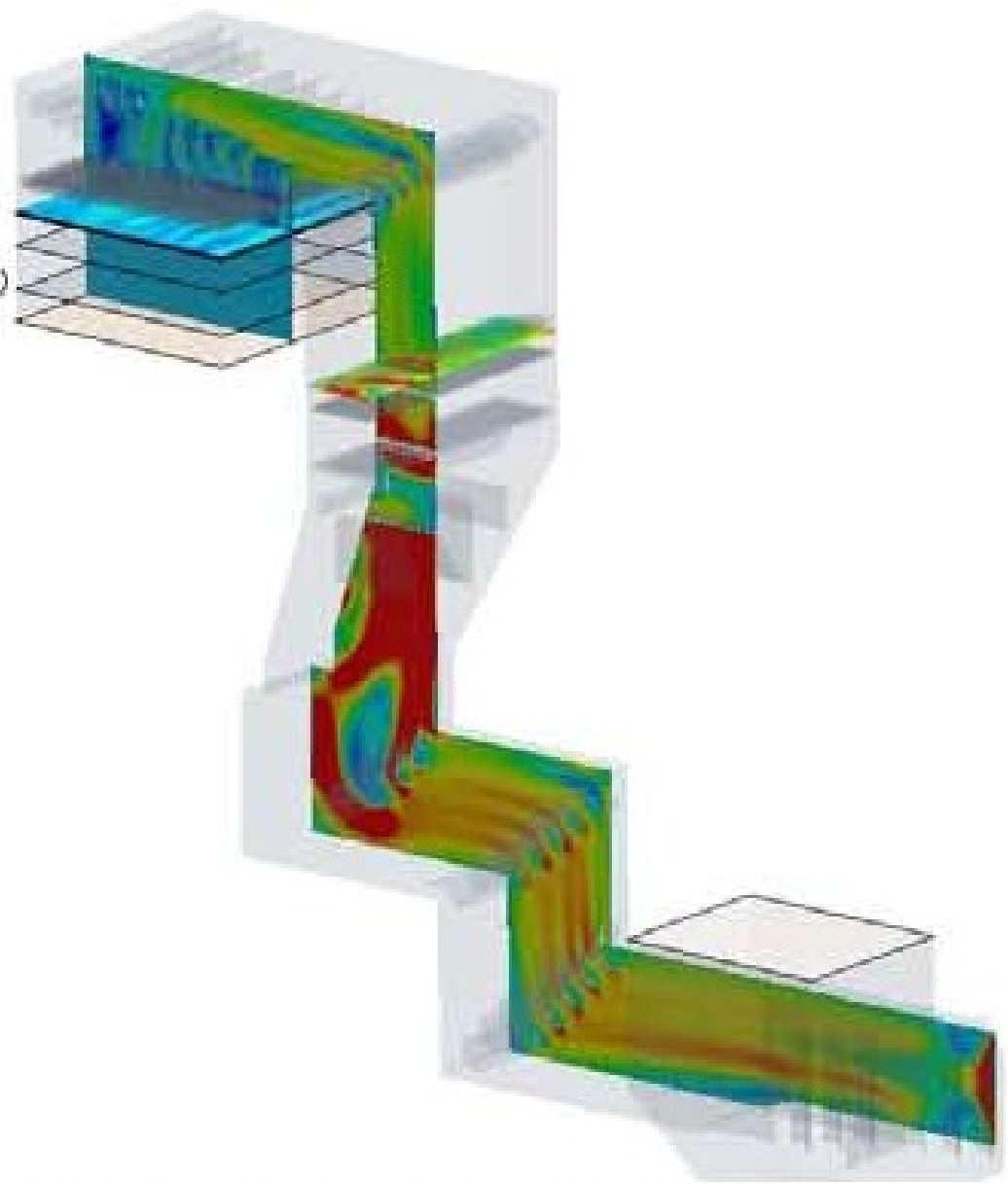


Figure 1: Baseline System Velocities

Bailly Unit 8 CFD Modeling Study

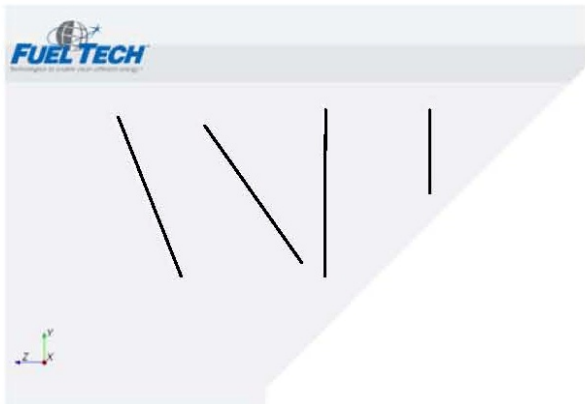


Figure 3: Expansion Vanes below AIG



Velocity: Magnitude (ft/s)

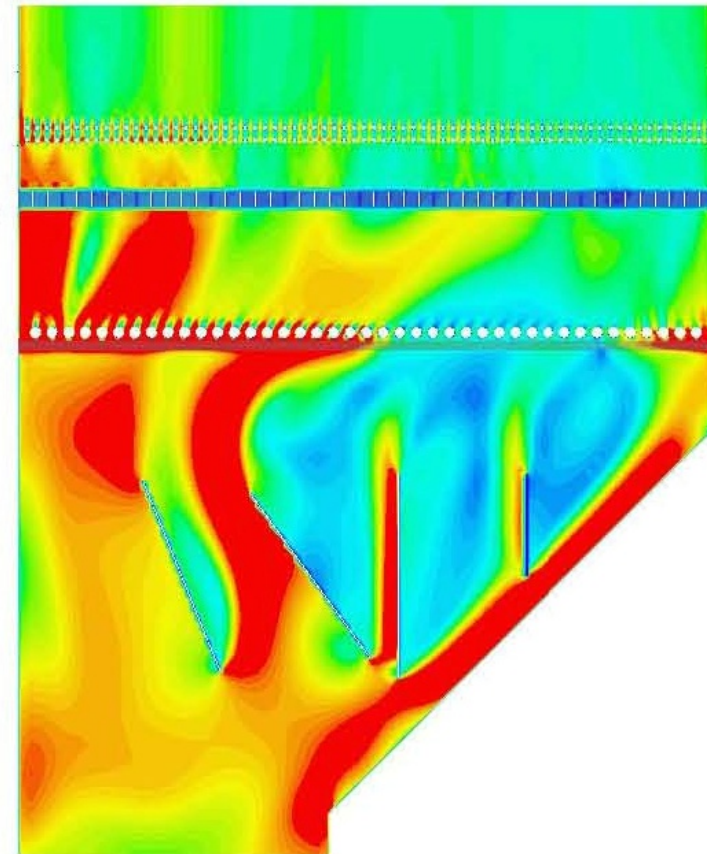
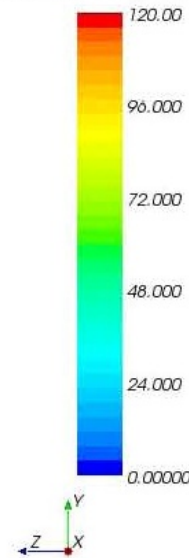


Figure 4: Velocities at Expansion Vanes Scale of 0 to 120 ft/s

Bailly Unit 8 CFD Modeling Study

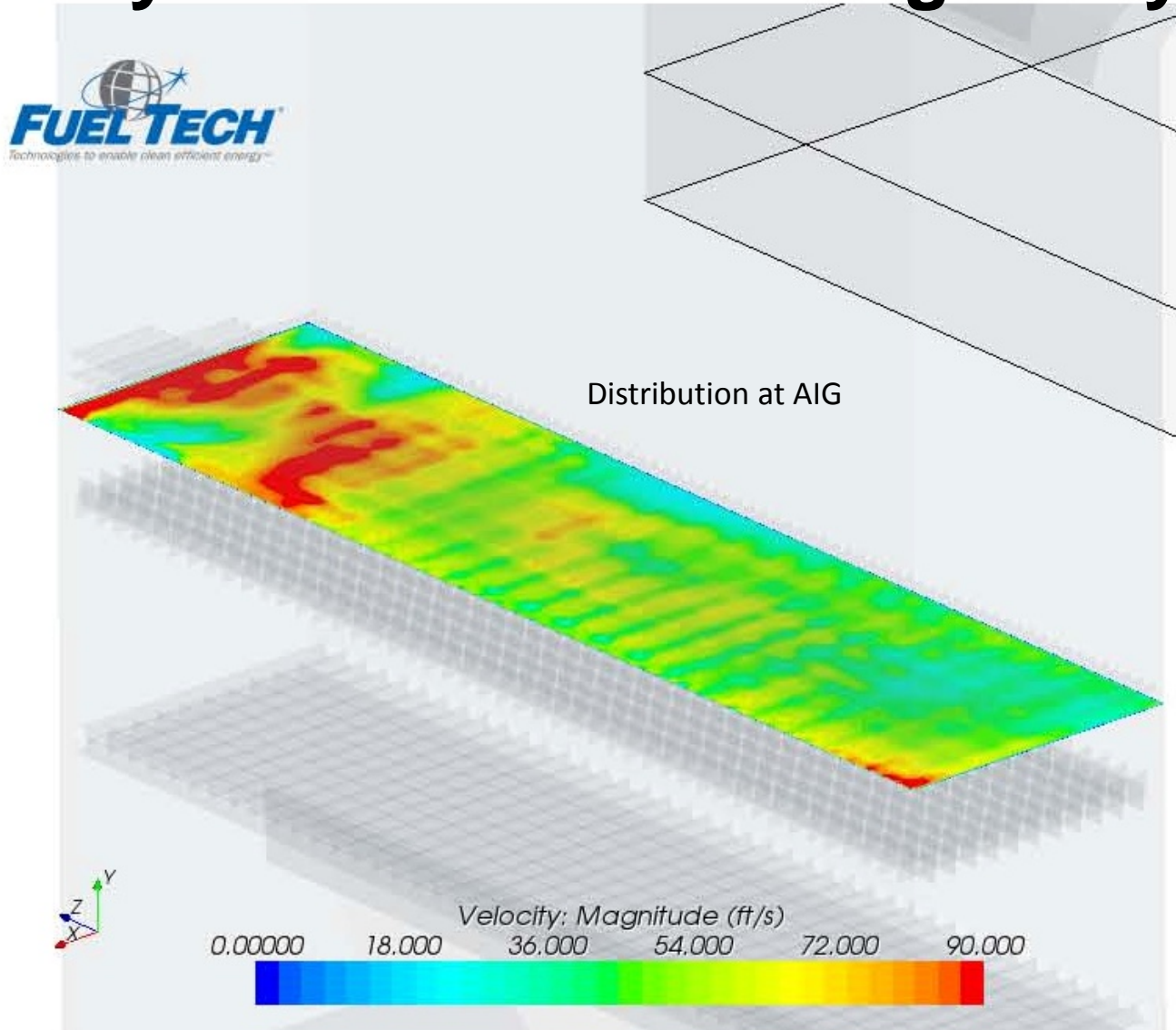
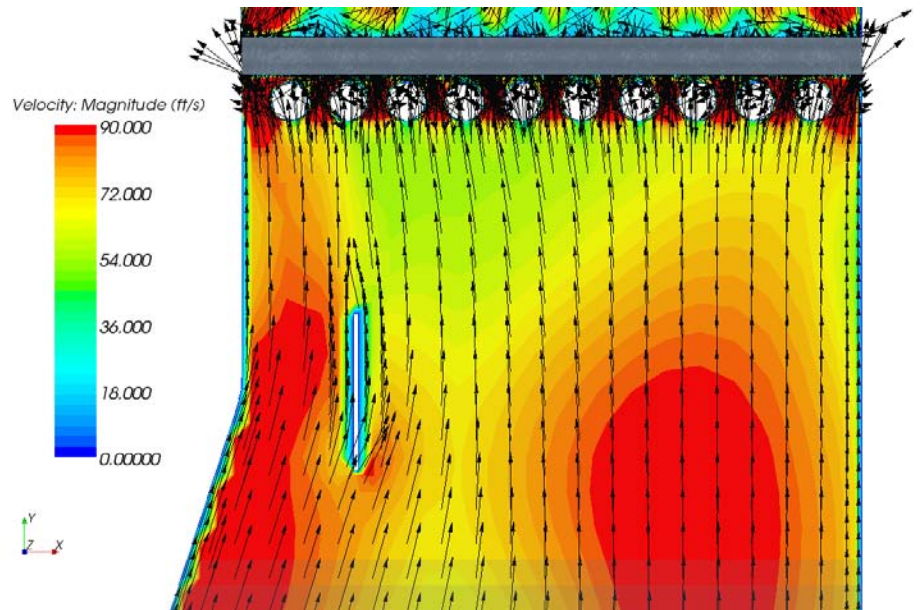


Figure 5: AIG Velocity Distribution

Bailly Unit 8 CFD Modeling Study



Bailly Unit 8 CFD Modeling Study

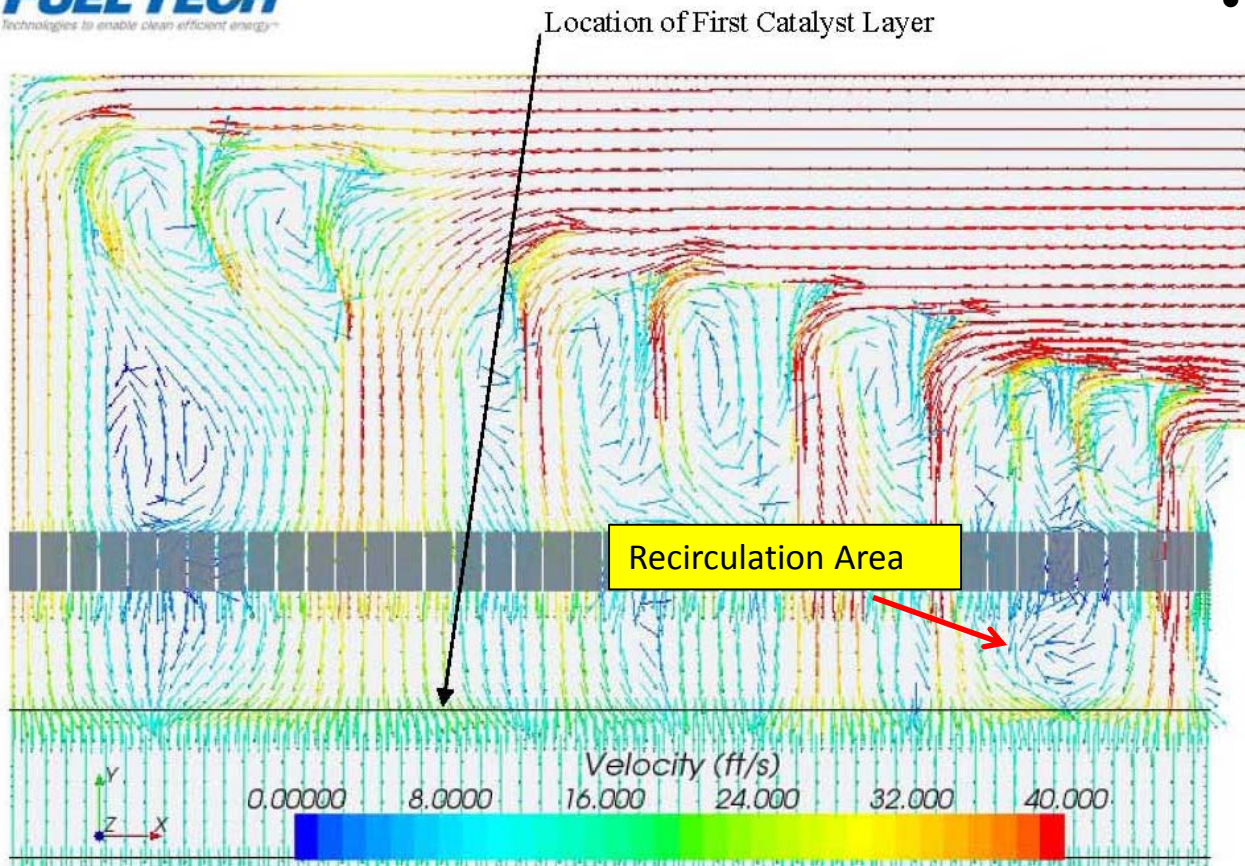
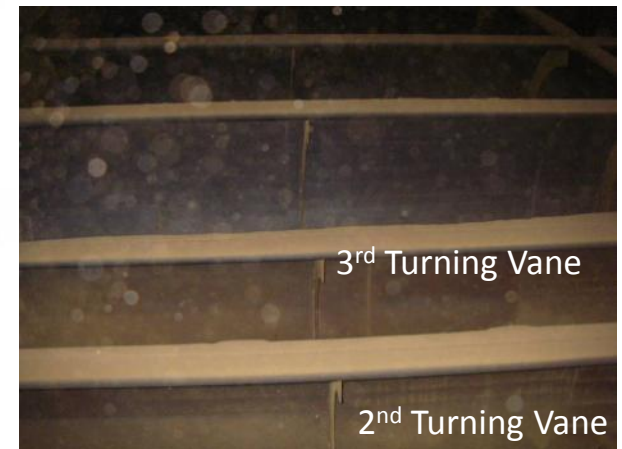


Figure 7: Vectors above Catalyst Scale 0 to 40 ft/s

- Flow Eddies Abundant Into L1 (Recirculation)



Bailly Unit 8 CFD Modeling Study

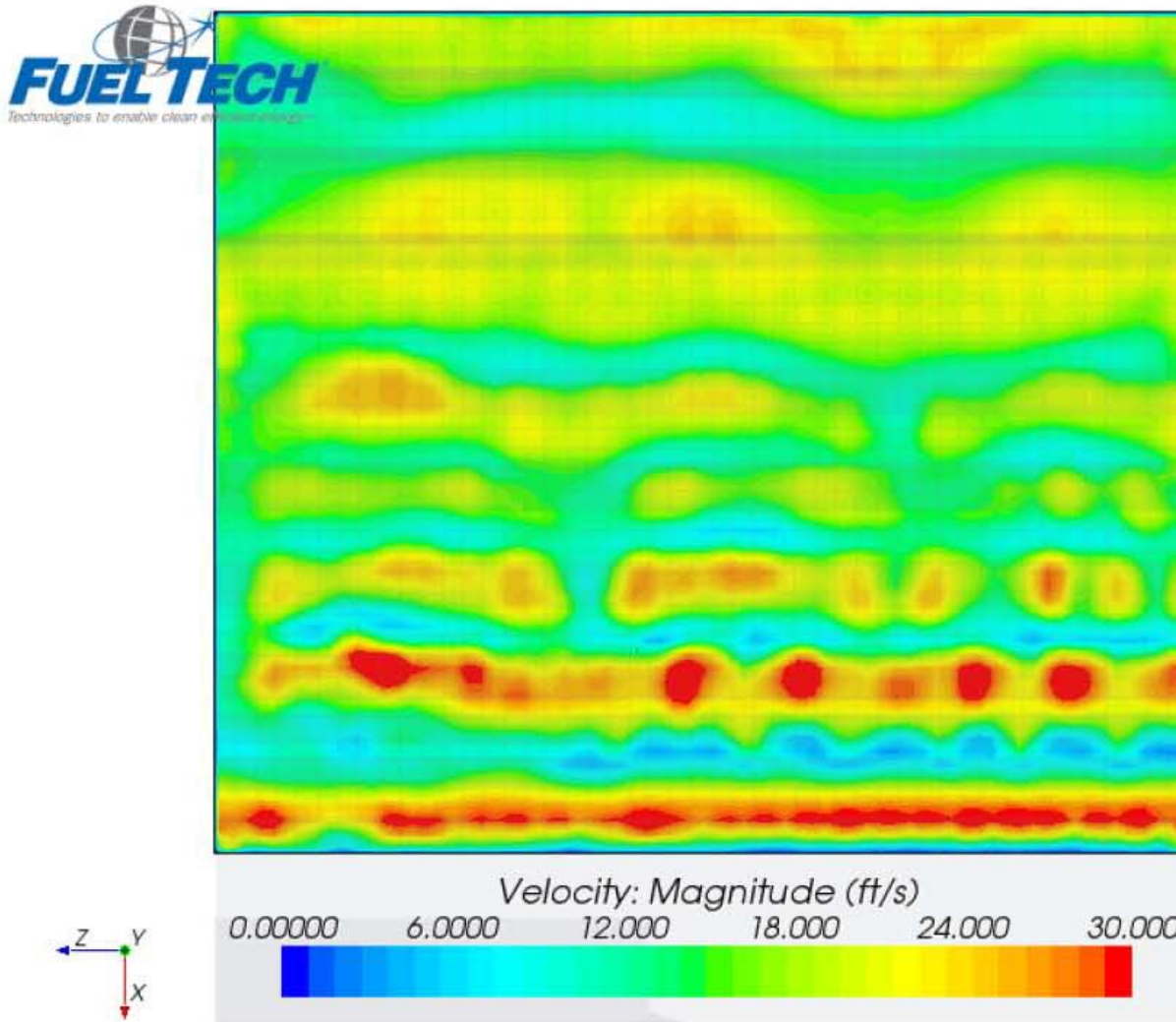


Figure 8: Velocity Distribution 6 inches above the Catalyst Face Scale 0 to 30ft

Bailly Unit 8 CFD Modeling Study

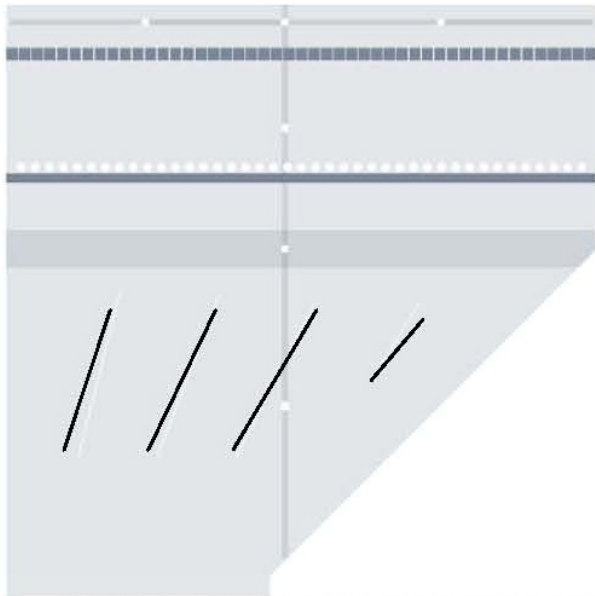


Figure 12: New Expansion Vane Geometry

- Relocated “Finger-Vanes” in Vertical Riser Duct

Figure 12: New Expansion Vane Geometry

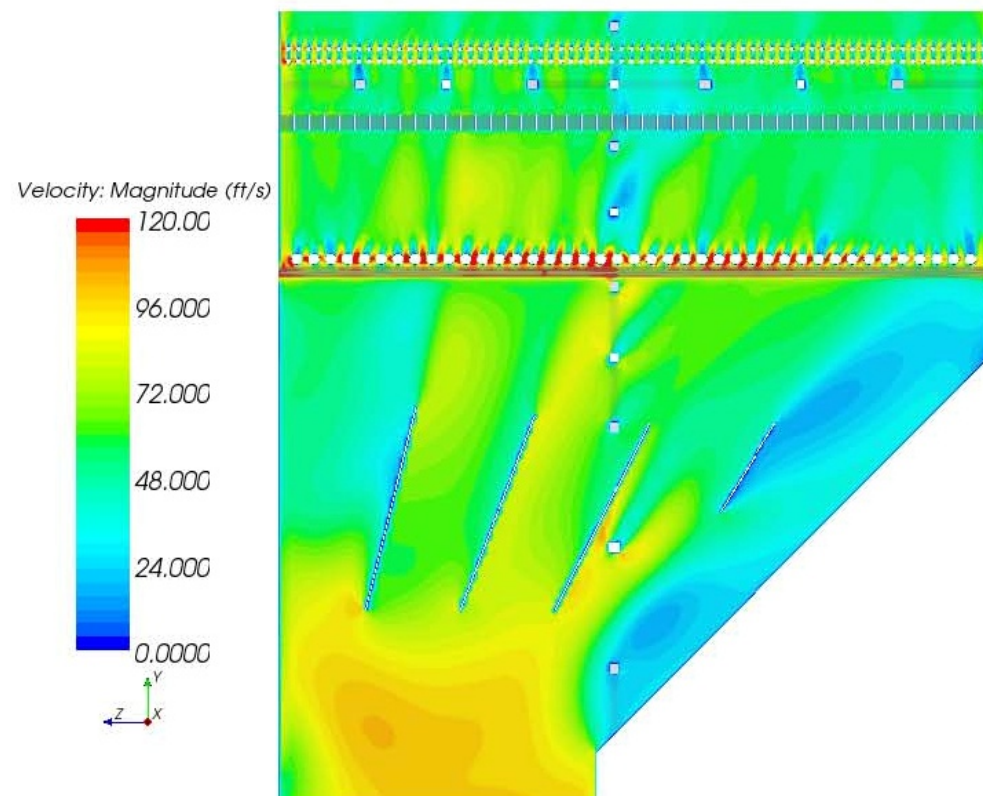


Figure 13: Velocities at Improved Expansion vanes

Bailly Unit 8 CFD Modeling Study

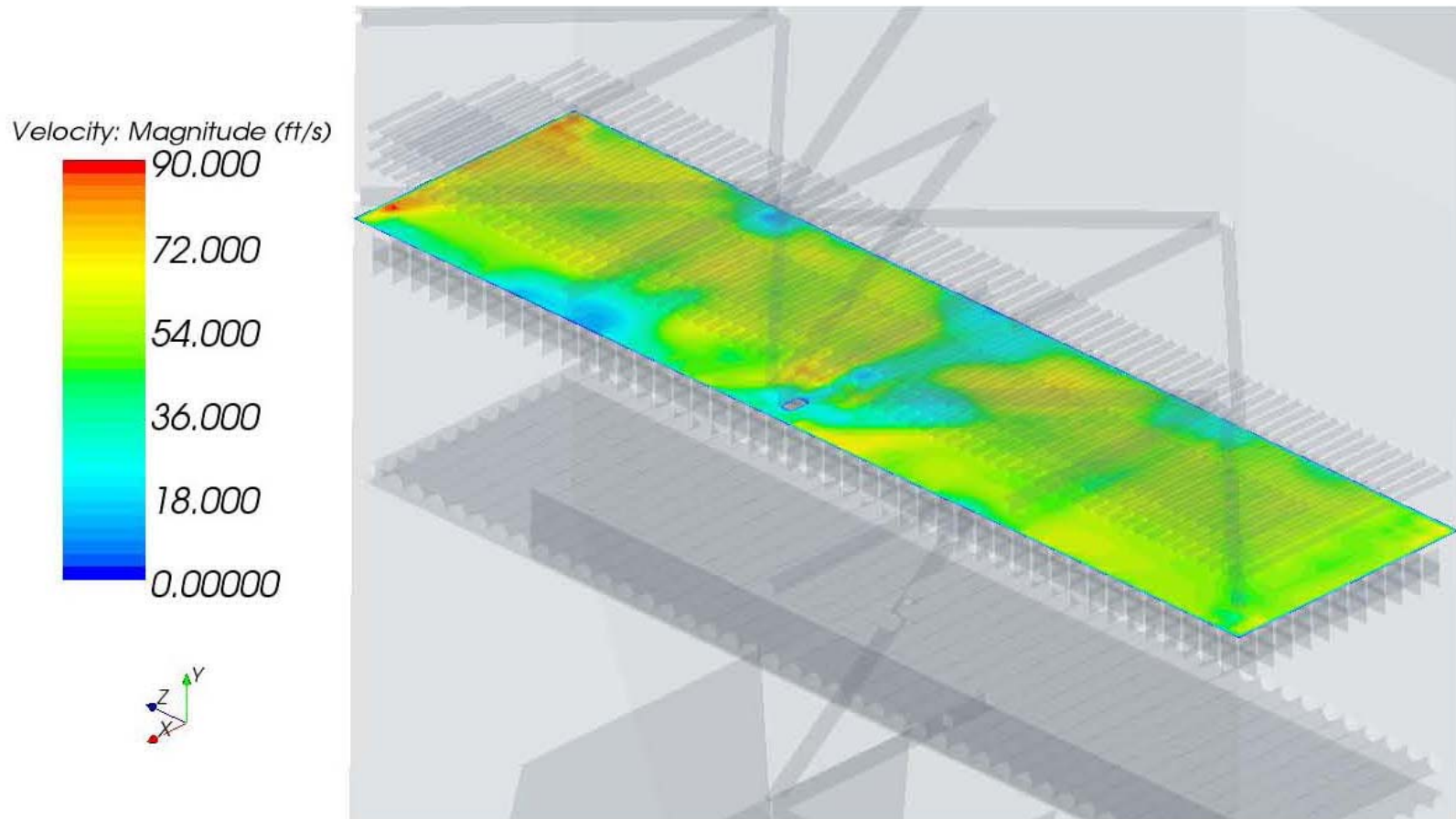
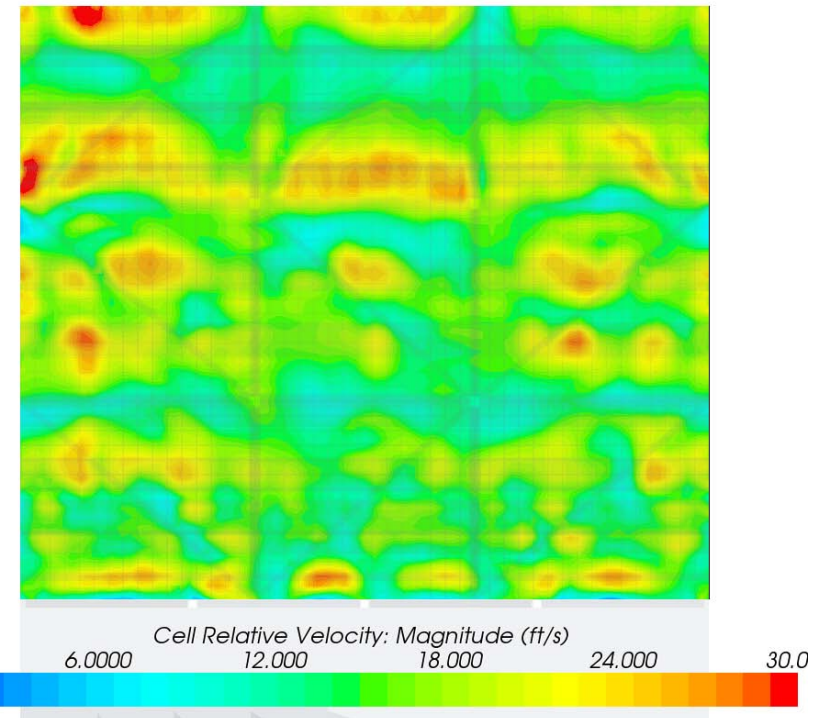
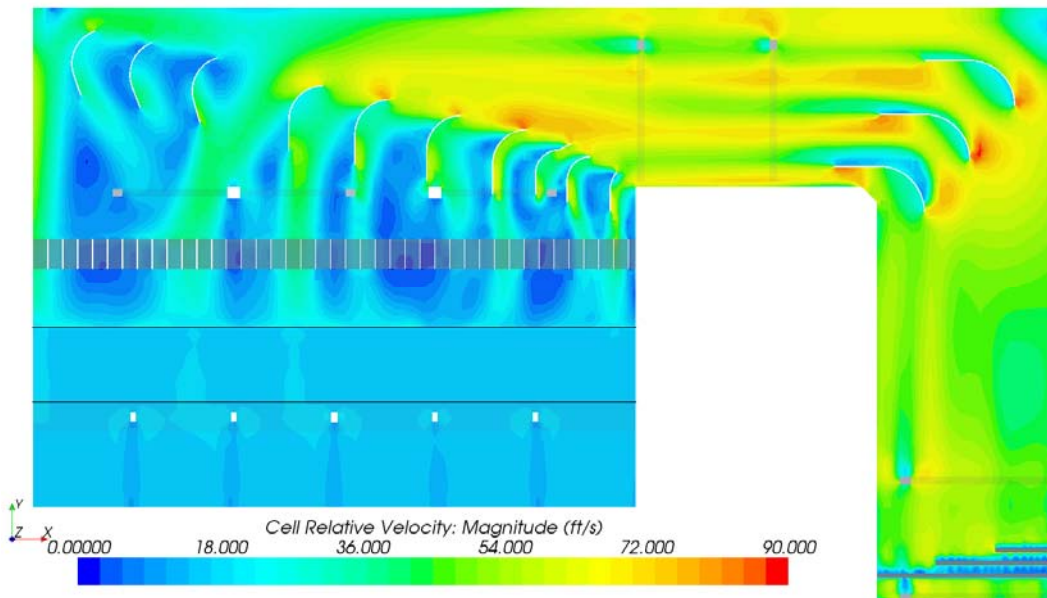


Figure 14: AIG Velocity Distribution

Bailly Unit 8 CFD Modeling Study

- Examined Change In Vanes Upstream of Crossover Duct
- High Velocity Exists That Sweeps Ash From Floor
- Relocated 2 Vanes; Improved Distribution By Minor Amount
- 35% of Points Within +/-15% of Average
- Expensive For Payback (Not Considered Any Further)



Bailly Unit 8 CFD Modeling Study

- Novel Solution: Trim 1st Vane and Extend 3rd Vane in Reactor Hood

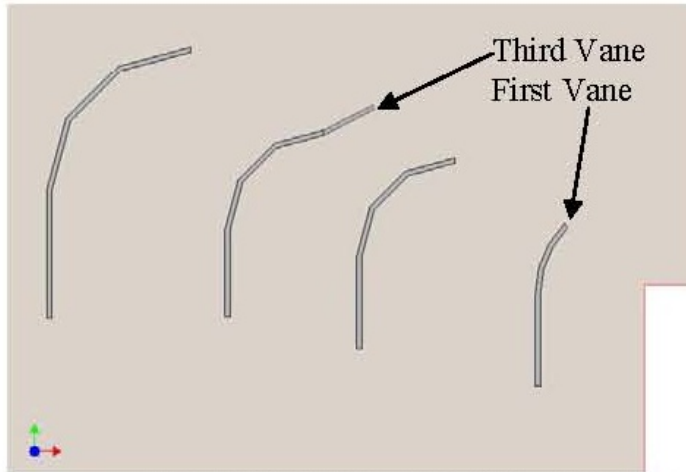


Figure 17: Vane Geometry Changes

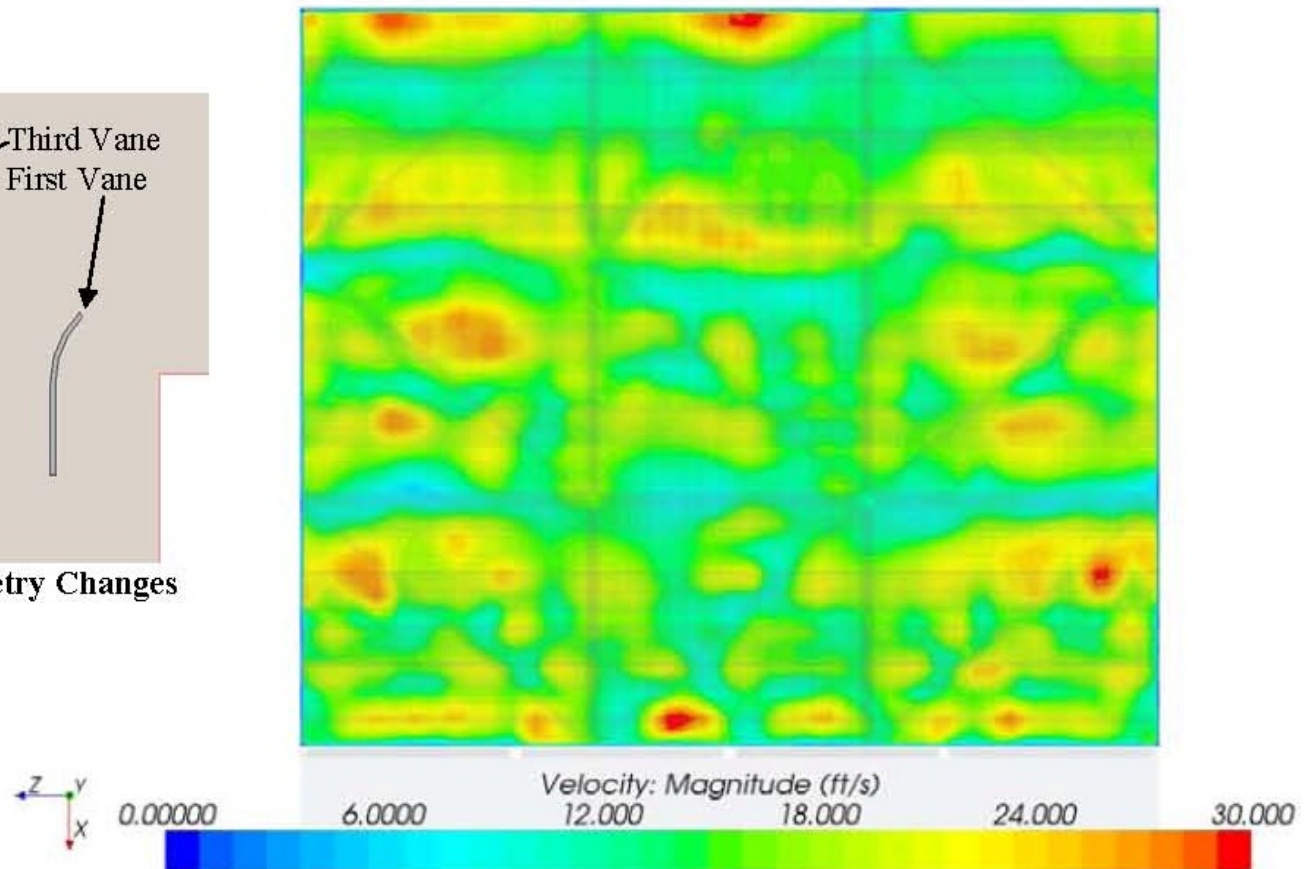


Figure 19: Velocity Distribution at Catalyst

Bailly Unit 8 CFD Modeling Study

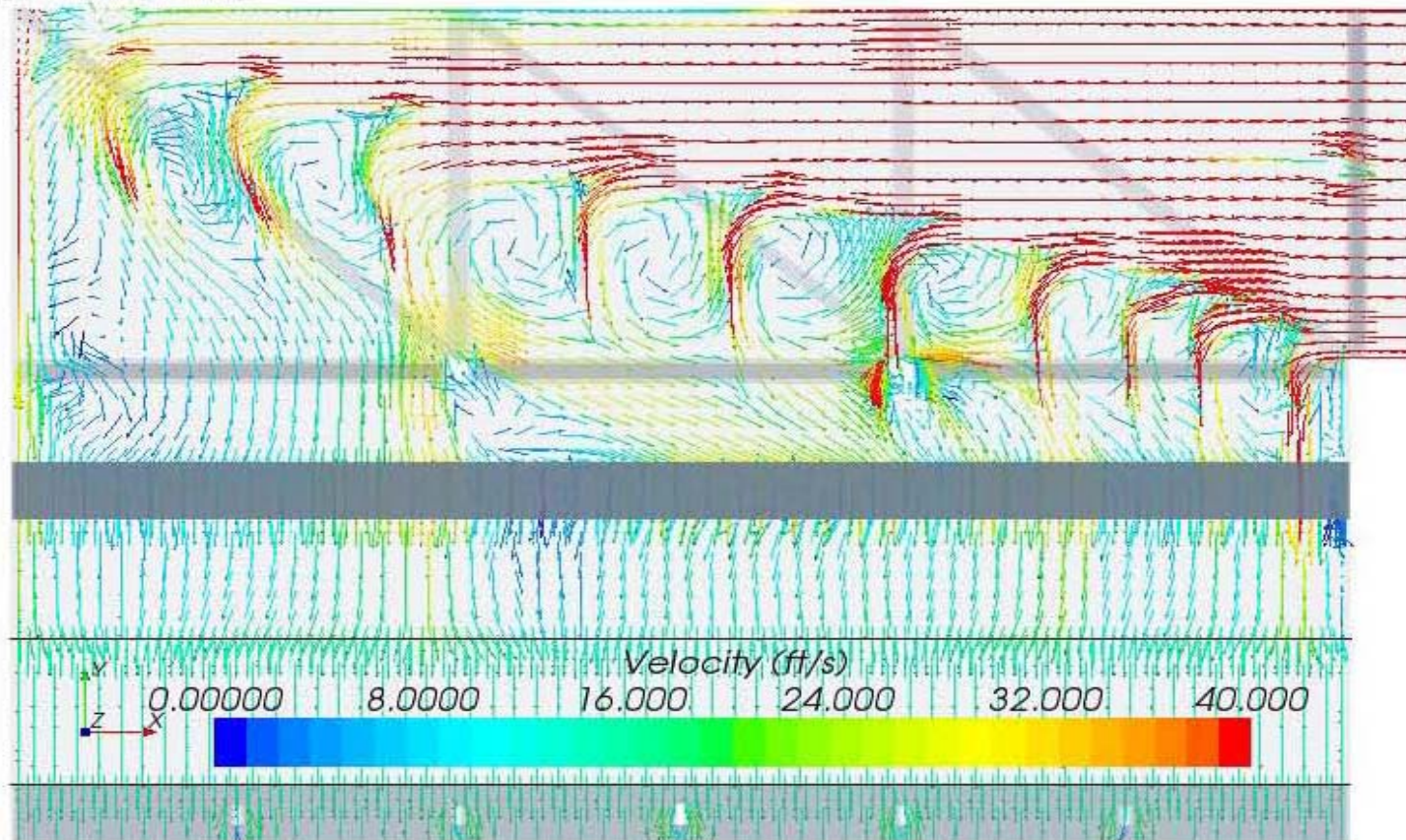


Figure 18: Vectors above Catalyst

Baily Unit 8 CFD Modeling Study

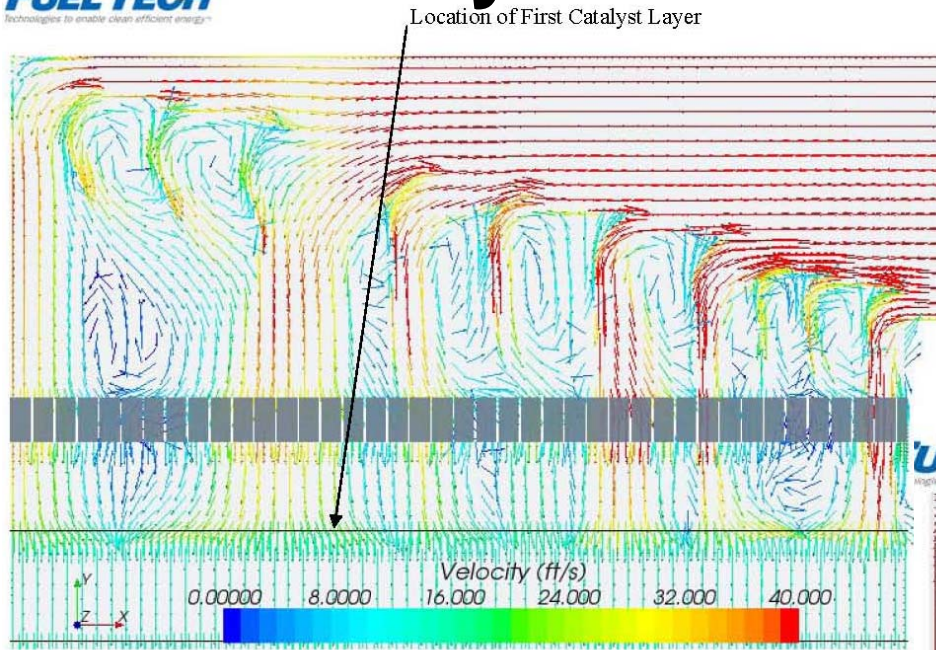


Figure 7: Vectors above Catalyst Scale 0 to 40 ft/s

Baseline

Recirculation Area
Removed

With Vane Modifications

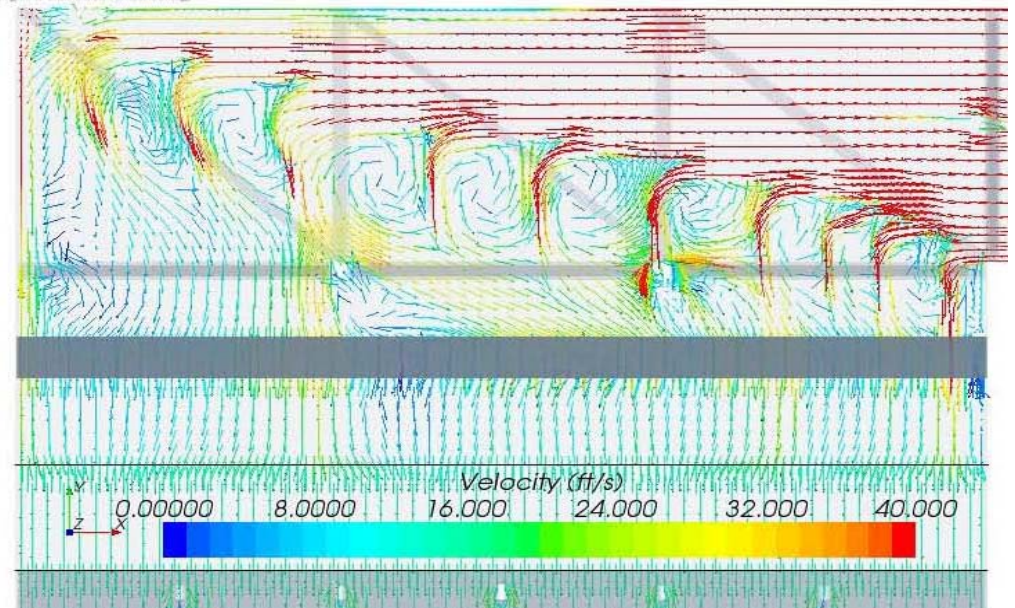
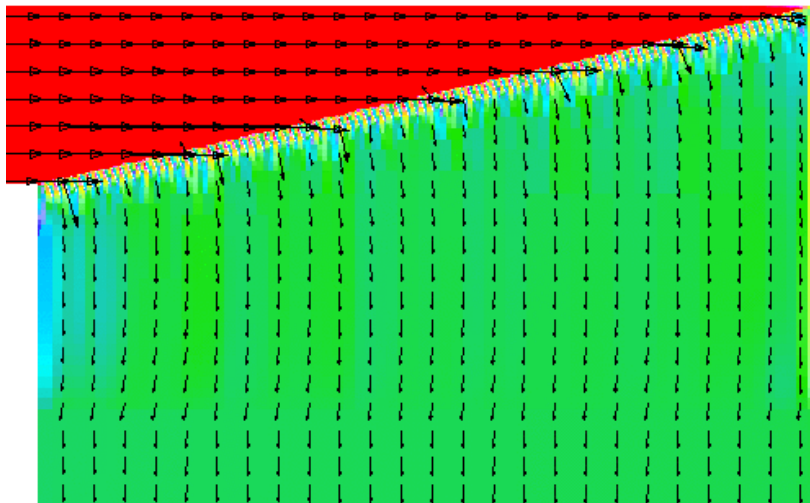


Figure 18: Vectors above Catalyst

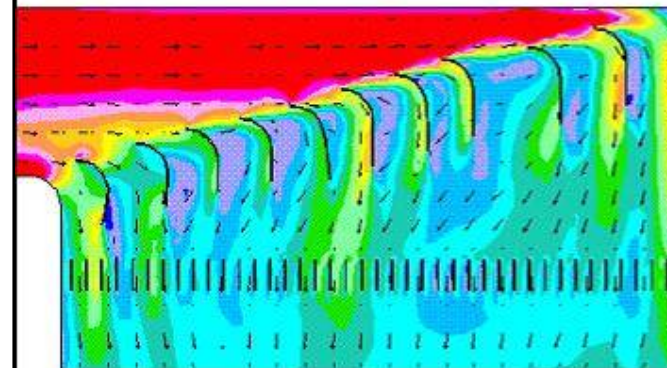
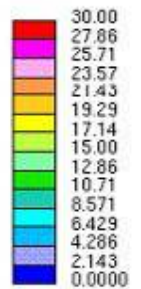
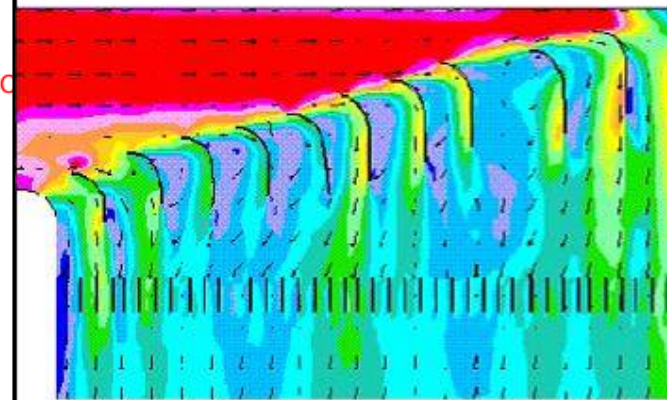
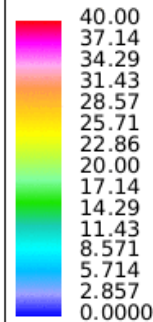
Example of GSG from CFD Modeling



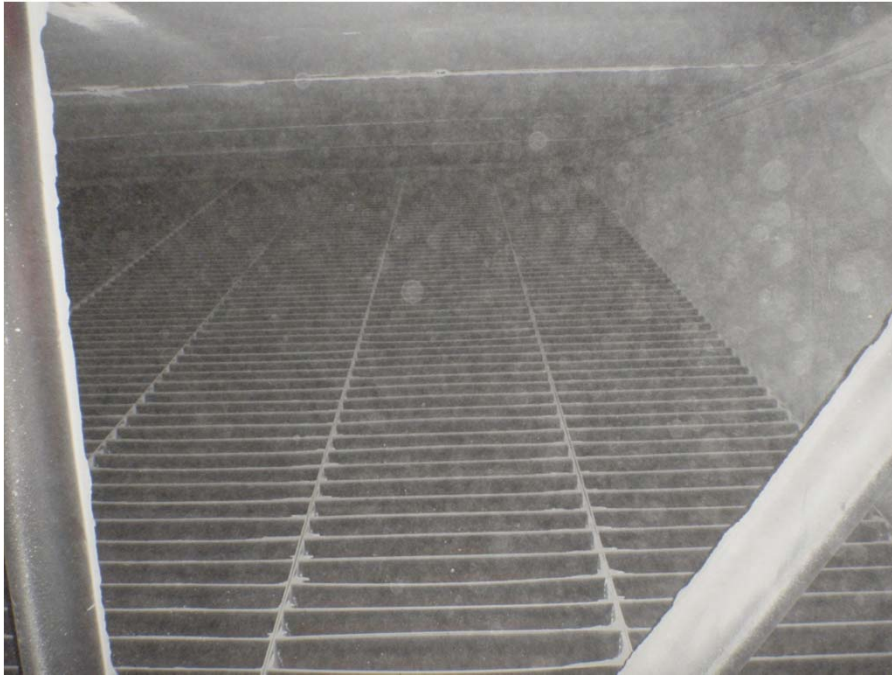
GSG = Graduated Straightening Grid
Patent Pending by Fuel Tech


FLOWTACK
pro-STAR 3.2

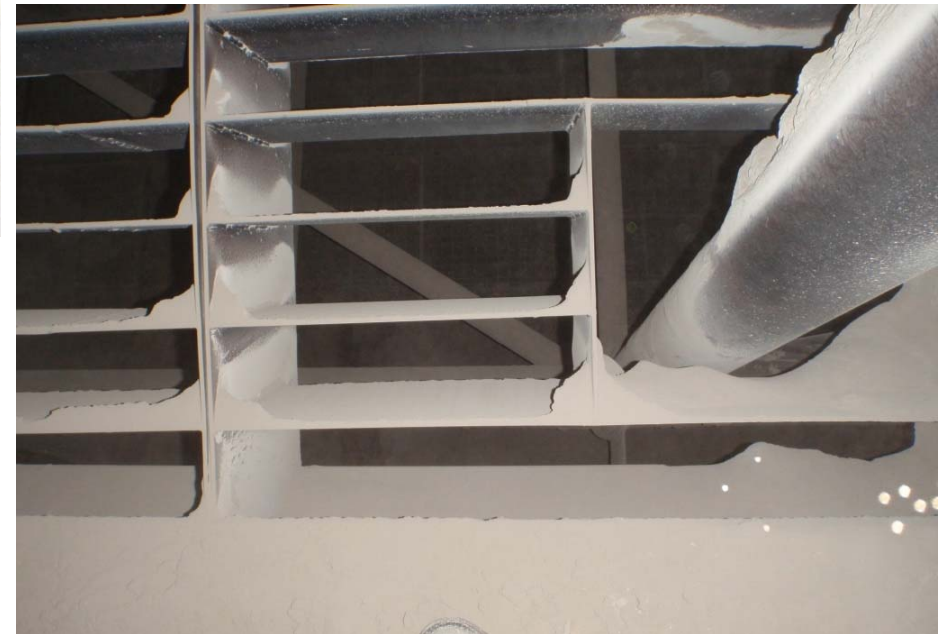
Velocity
Ft per sec
*PRESENTATION



Example of GSG from PRB Fired Unit



GSG = Graduated Straightening Grid
Patent Pending by Fuel Tech



Bailly Unit 8 CFD Modeling Study – Goal of Study to Improve Flow Distribution

- CFD Modeling Performed by Fuel Tech, Inc.
- CFD Baseline Demonstrated High Velocity Distribution (Approx 43.5%)
 - Flue Gas Distribution Upstream AIG = 100% of points within 15% of mean
 - Flue Gas Distribution Upstream Catalyst = 100% of points within 15% of mean
- Relocated “Finger-Vanes” in Vertical Riser Duct
- Trim 1st Vane and Extend 3rd Vane in Reactor Hood (“Economical Solution”)
- Relocate Greater Number of Vanes or Install Graduated Straightening Grid (GSG) or Similar Device (Options Results in Substantial Cost Increase)
- Low Load Checked & CFD Showed No Issues




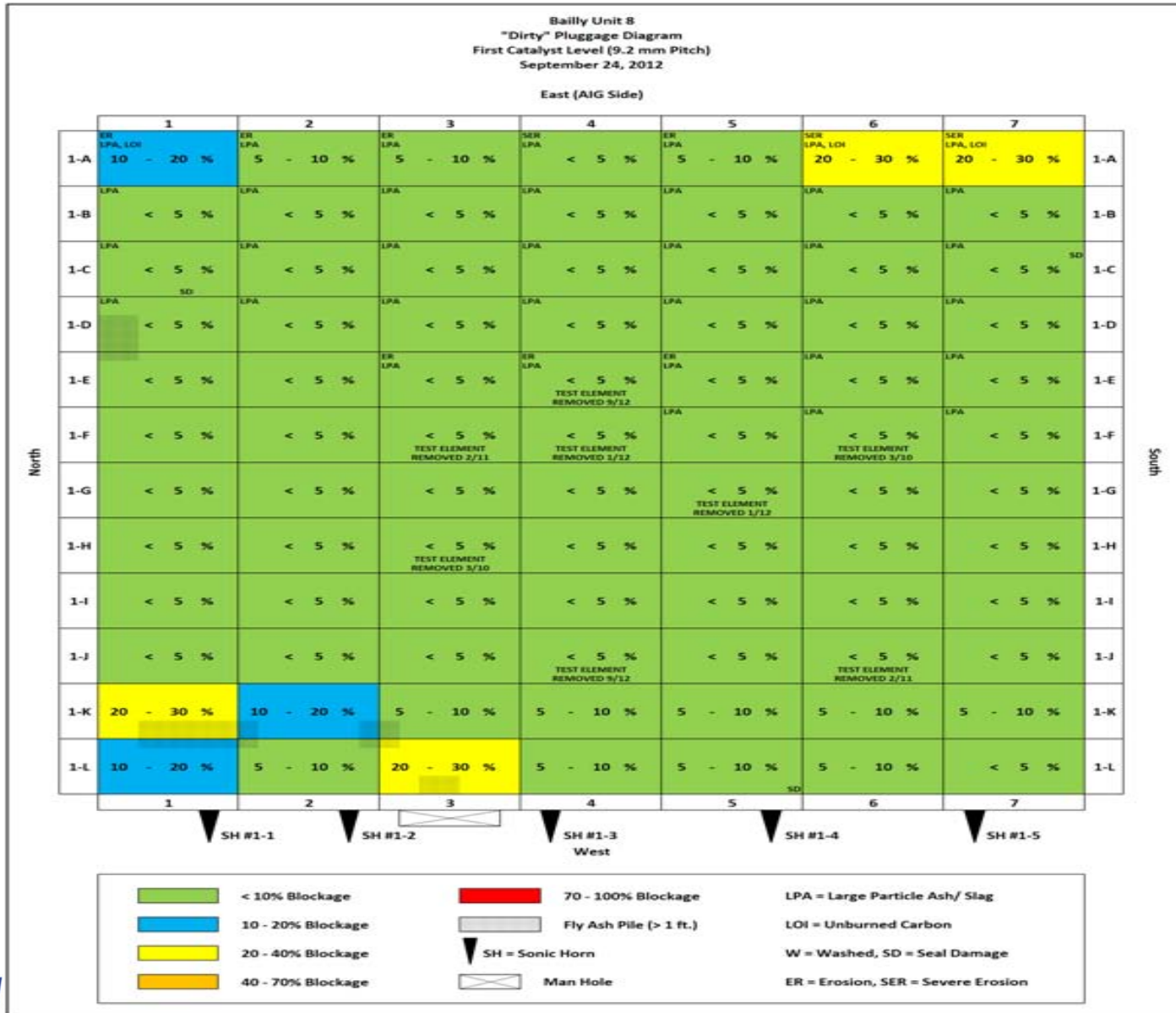
Summary	% with in 10 %	% with in 15	RMSE
Run			
Baseline (existing configuration)	15.3	23.9	43.5
AIG Expansion Vane change	20.1	 30.5	34.6
Crossover Vane change	19.4	 32.4	35.3
Reactor Hood vane change	24.2	 34.5	31.0
Crossover and Reactor Vane change	23.7	34.9	31.0

Table 1: Velocity Statistics at Catalyst

Bailly Unit 8 Inspection Results Overview

- Avg pluggage L1 = 5% (9.2 mm; 17.2k hrs), L2 pluggage = 3% (8.2 mm; 8k hrs), L3 pluggage = >25% (6.7 mm; 35.4k hrs) (L3 Removed in Fall 2012)
 - Larger Pitch Effective in Mitigating Pluggage in Combination to Guide Vane Modifications Upstream of AIG and Reactor Hood
- Top 9.2 mm Acting as Catalyst/Flow Rectifier. 1-2 ft Piles Observed L1 Northwest Corner For First Time (Approx. 17,200 hrs)
- Large Particle Ash (LPA) Observed On L1 and L2
 - LPA Screen Sections Are Worn (Replacement Recommended)
 - LPA Screen; “Fixed” Into Position & Does Not Move
- Unburned Carbon Observed in Reactor
- Fly Ash Piles (3-4 ft) observed on L3 (East side and NW side); L3 Removed
- Fly Ash Buildup Minor North Side of AIG Lances
- Erosion On East Side of L1 Due to High Velocities & Off Axis Velocity Vectors; Examine CFD Results For Solution

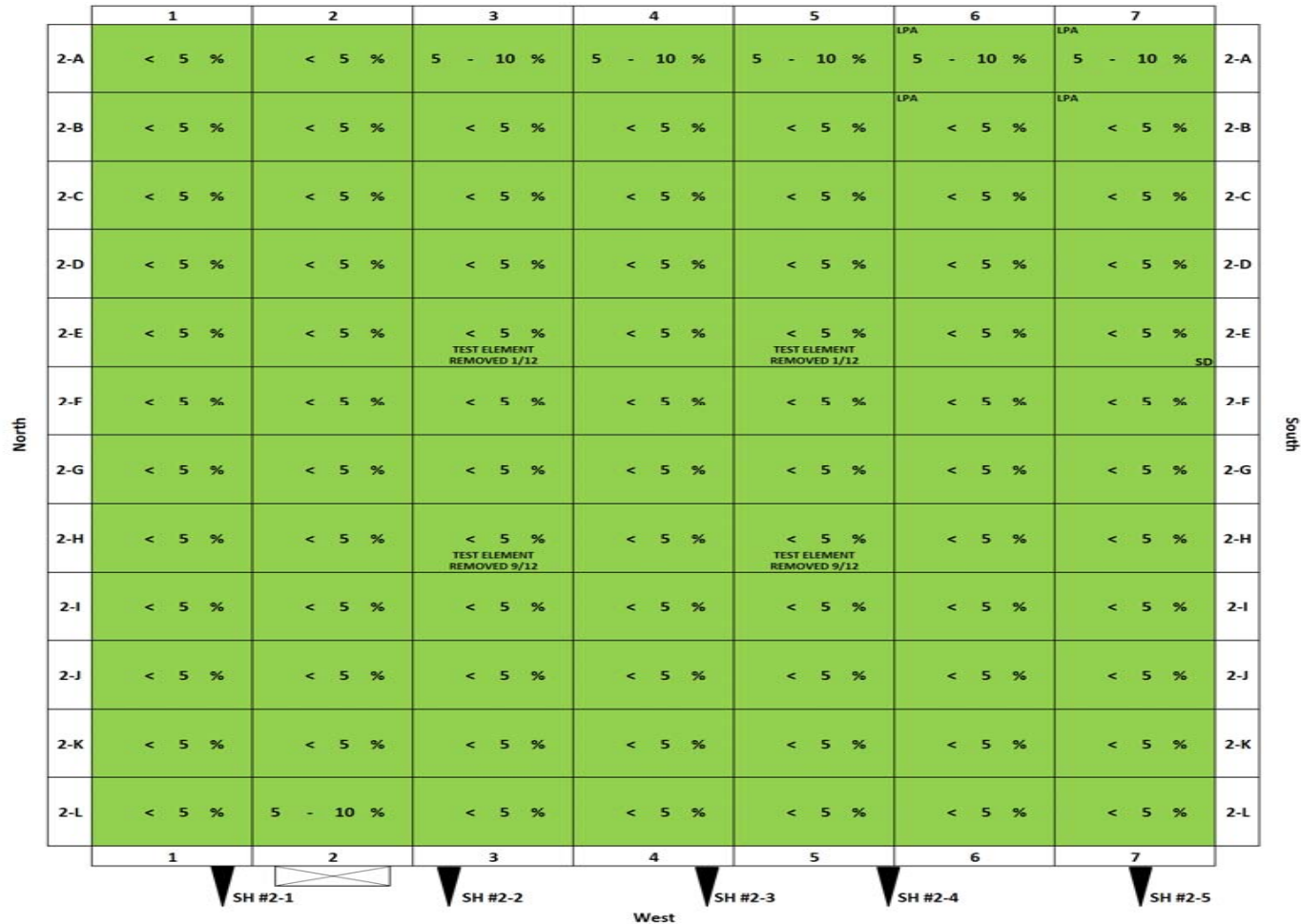
Bailly Unit 8 Reactor Inspection



Bailly Unit 8 Reactor Inspection

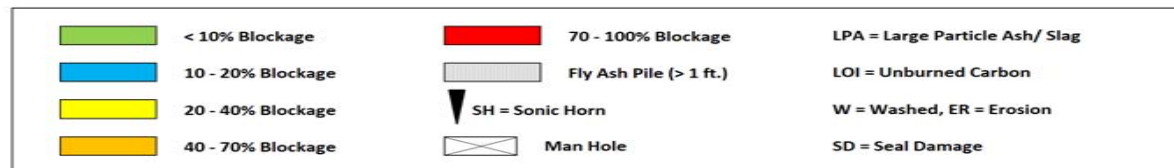
Bailly Unit 8
 "Dirty" Pluggage Diagram
 Second Catalyst Level (8.2 mm Pitch)
 September 24, 2012

East (AIG Side)



North

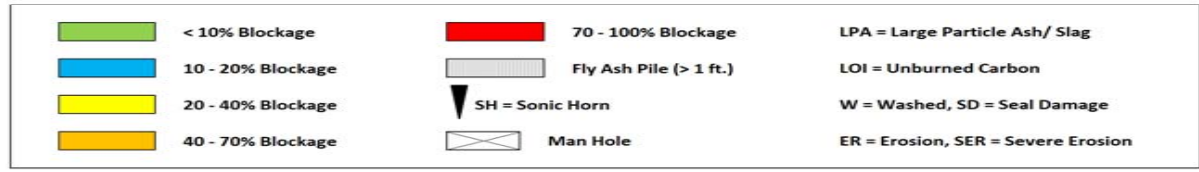
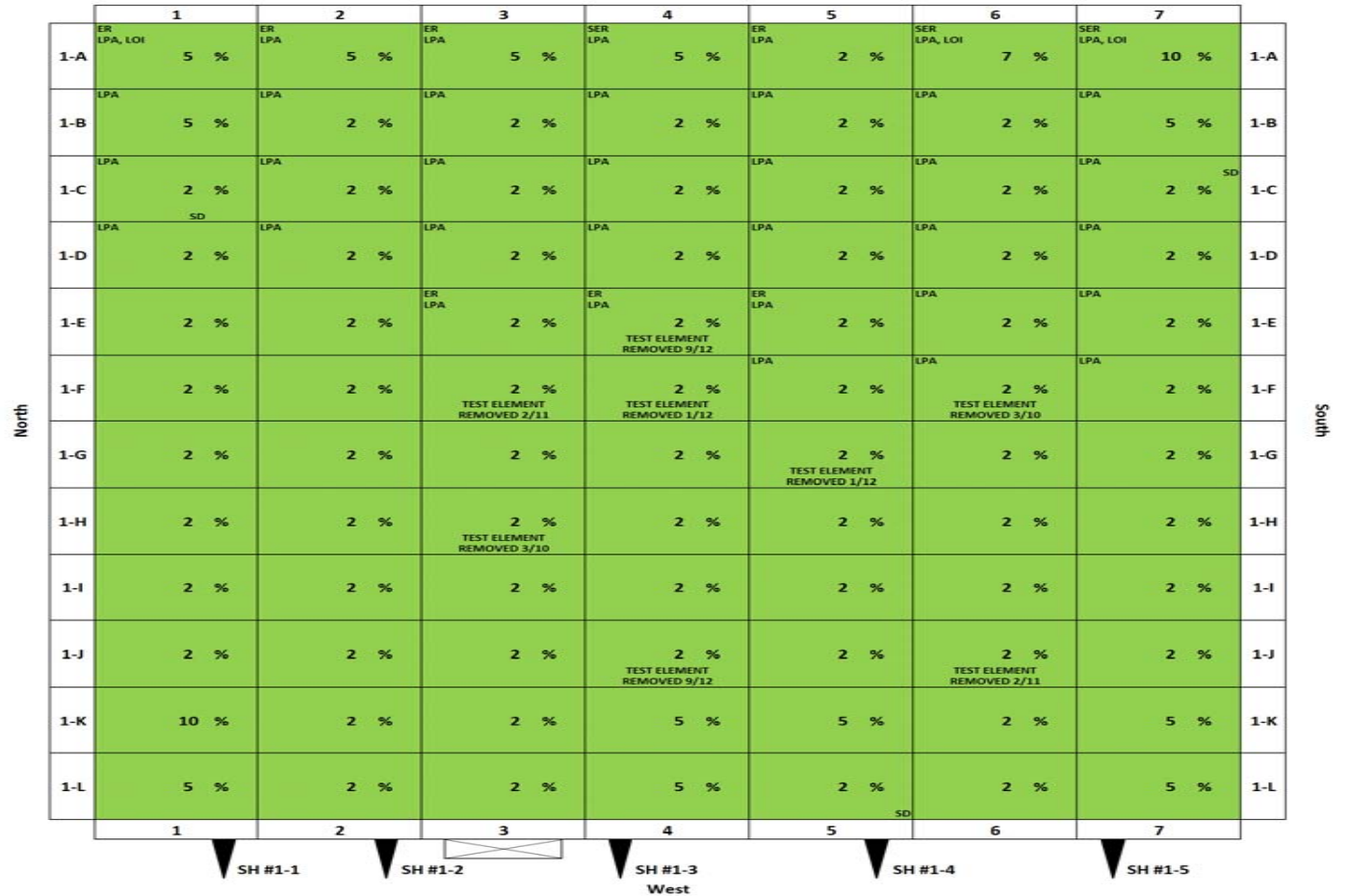
South



Bailly Unit 8 Reactor Inspection

Bailly Unit 8
 "Clean" Pluggage Diagram by NIPSCO
 First Catalyst Level (9.2 mm Pitch)
 October 23, 2012

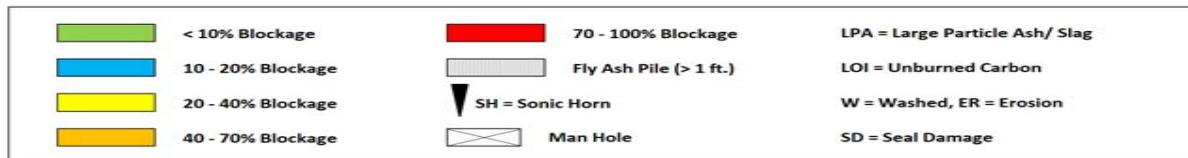
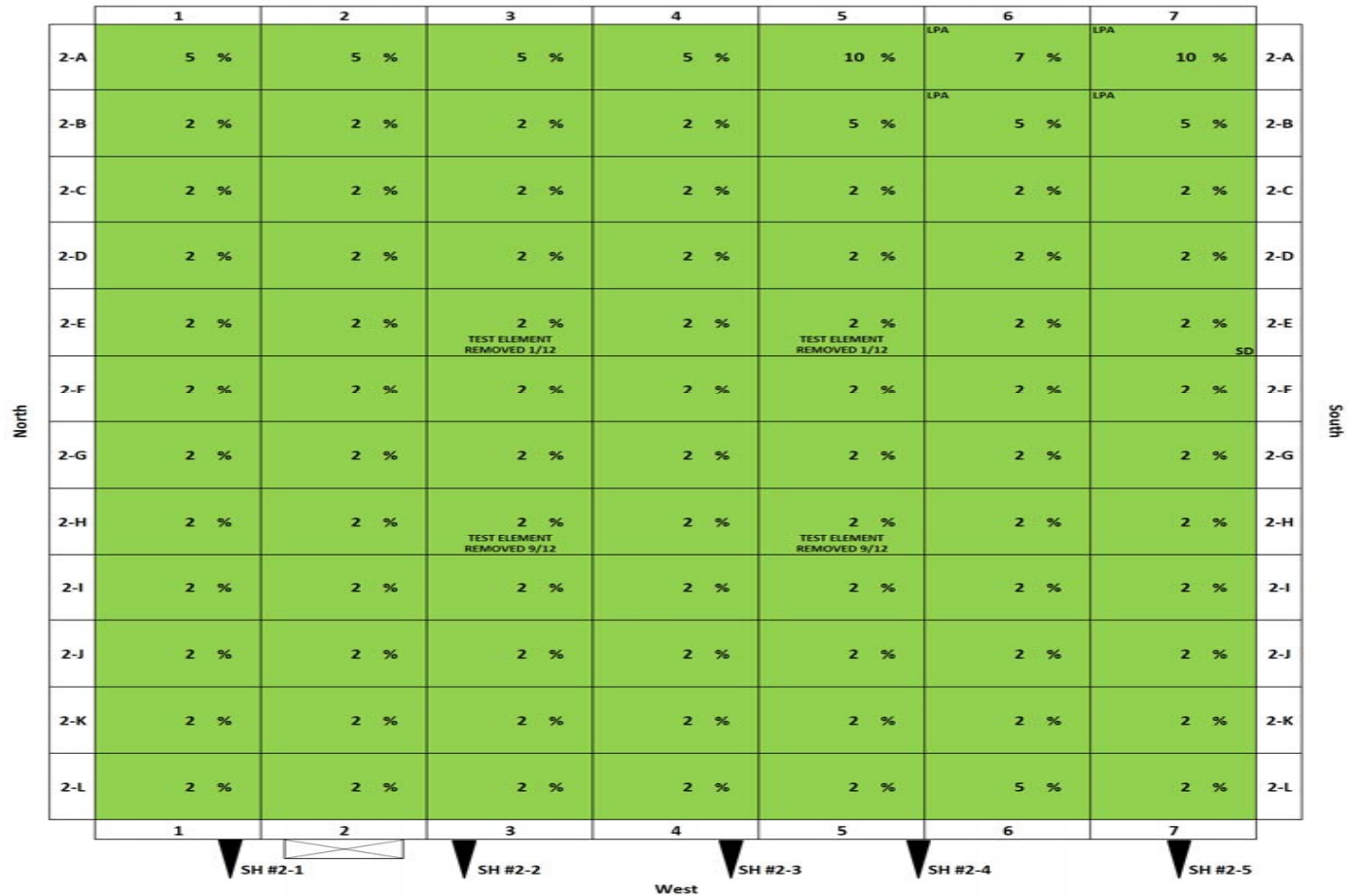
East (AIG Side)



Bailly Unit 8 Reactor Inspection

Bailly Unit 8
 "Clean" Pluggage Diagram (by NIPSCO)
 Second Catalyst Level (8.2 mm Pitch)
 October 23, 2012

East (AIG Side)

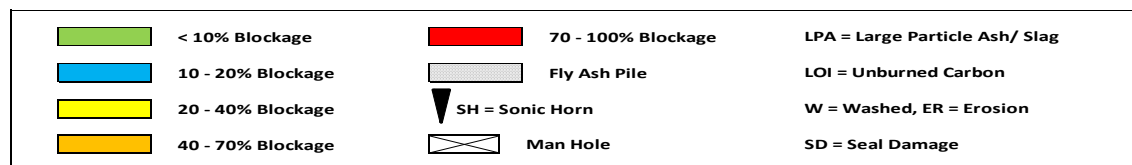
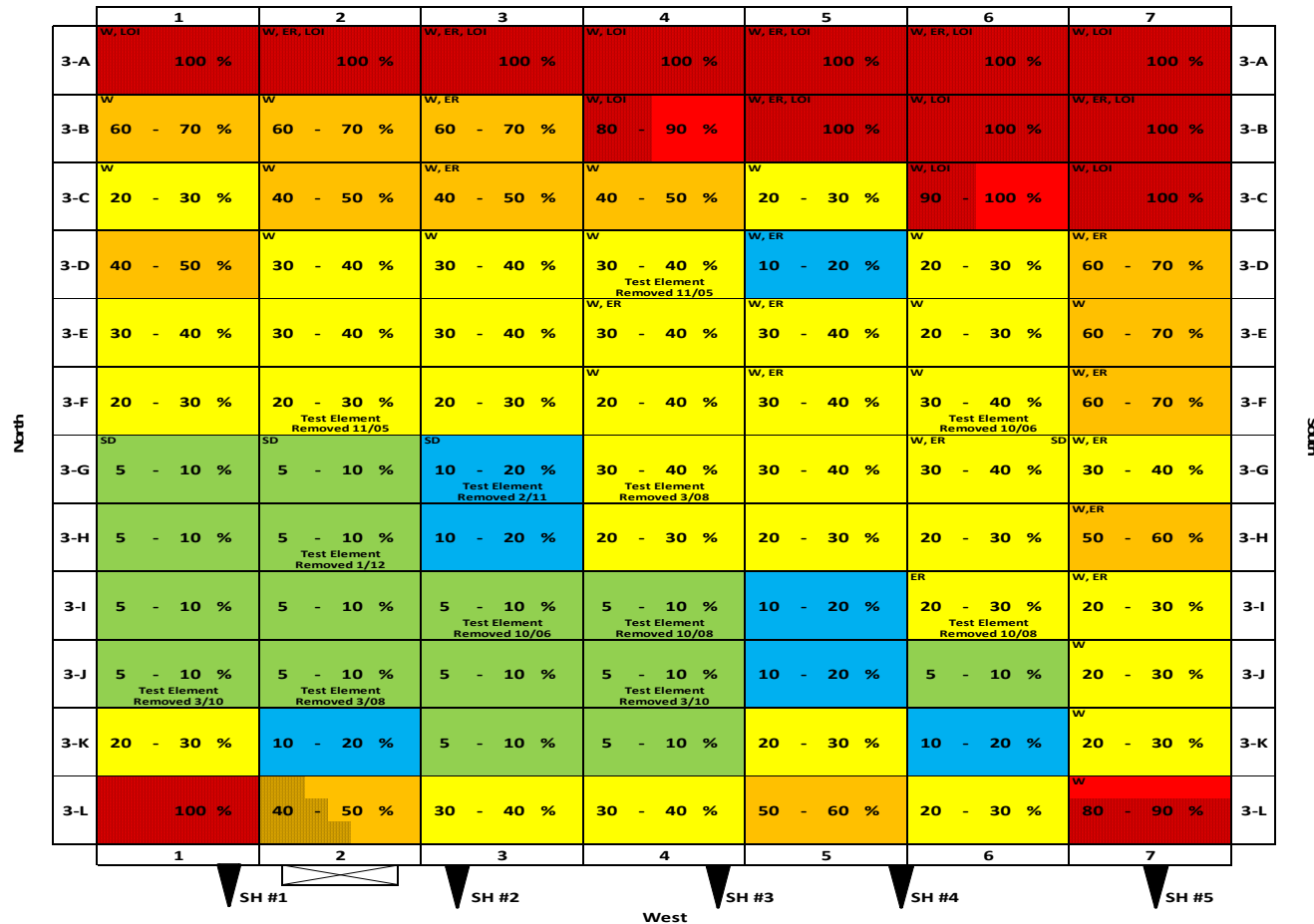


Bailly Unit 8 Reactor Inspection

Bailly Unit 8
Pluggage Diagram
Third Catalyst Level (6.7 mm Pitch)
January 30-31, 2012

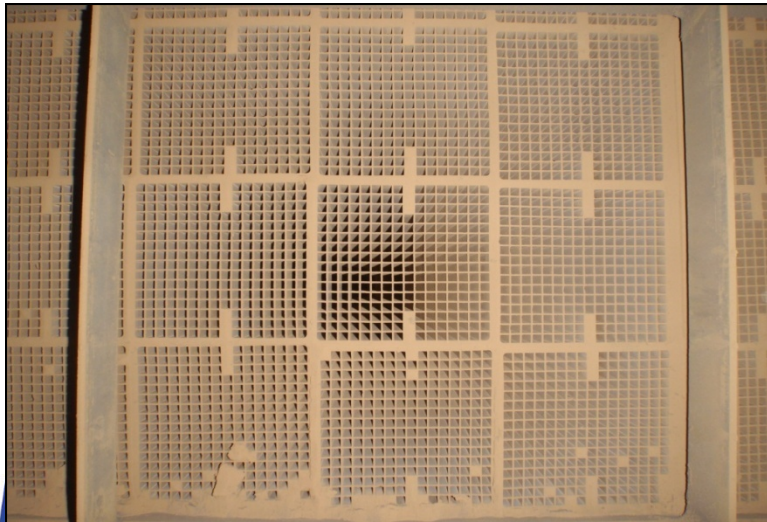
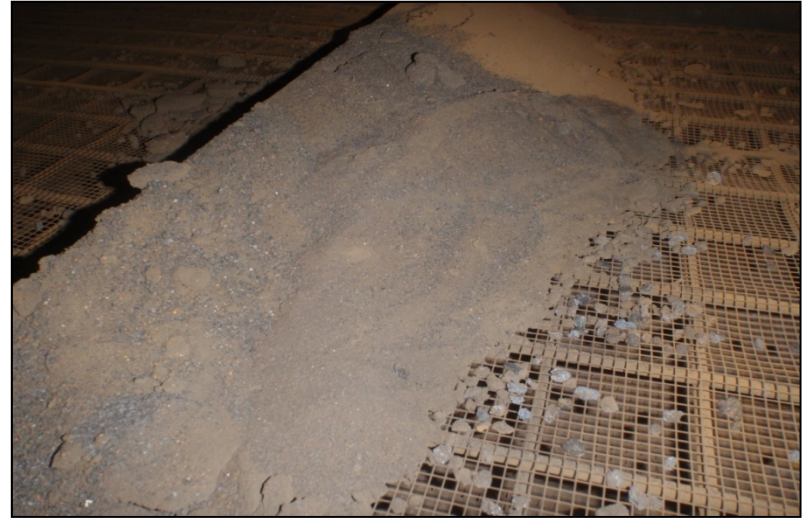
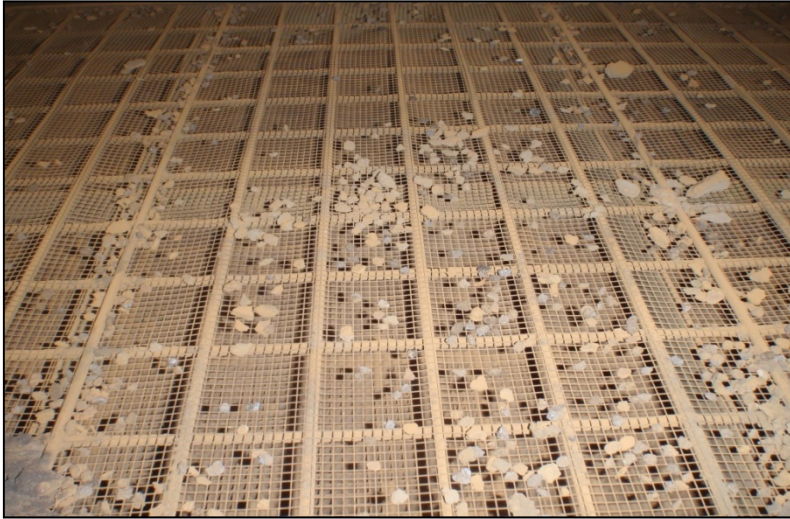
L3 Removed Fall 2012
Lower Pressure Drop

East (AIG Side)



Bailly Unit 8 Inspection Results Overview

Level 1



NW Corner

Bailly Unit 8 Inspection Results Overview



Level 1 (17,200 hrs)

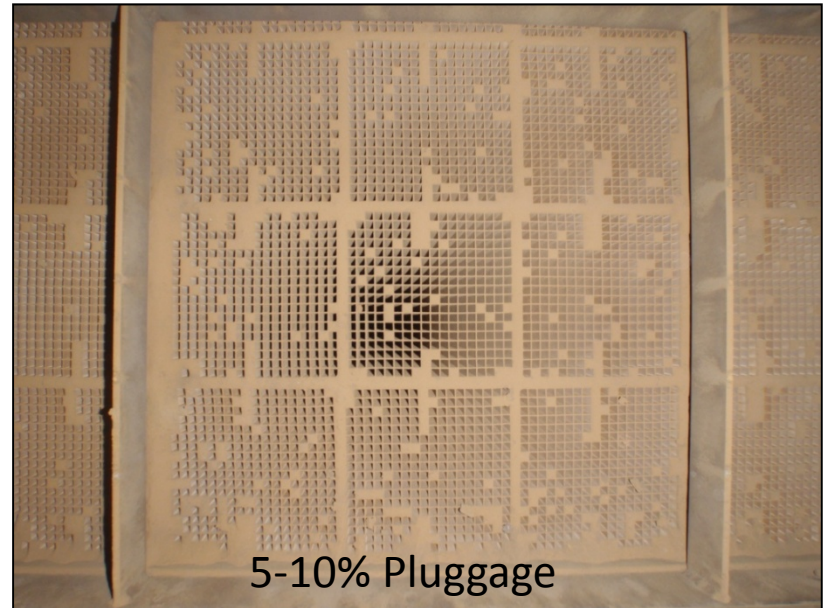
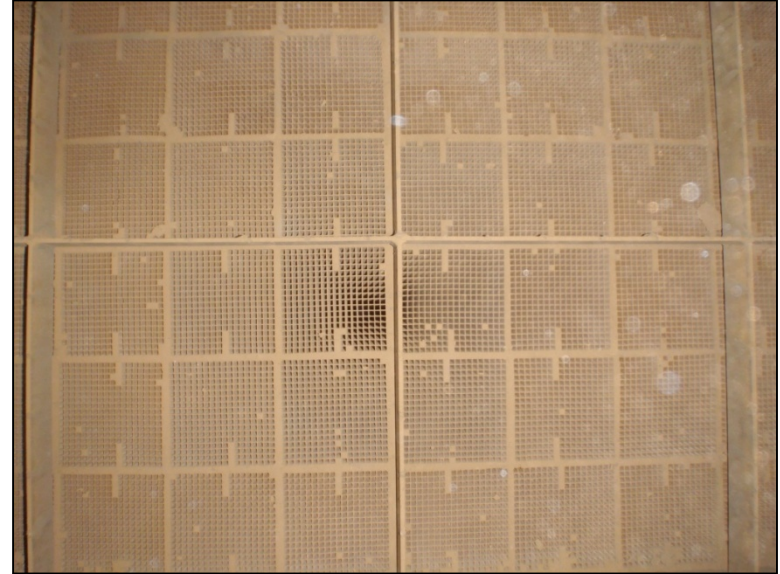


Erosion on East Side (AIG Side)

Bailly Unit 8 Inspection Results Overview



Level 2

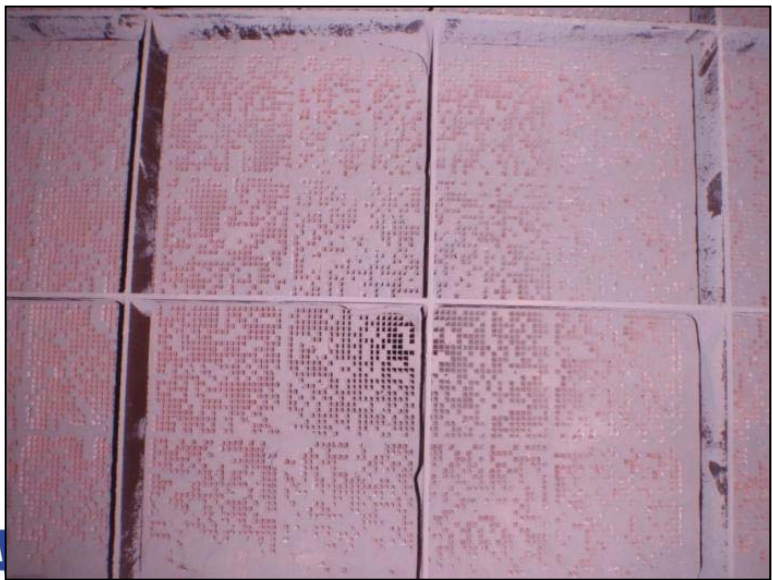


5-10% Pluggage

Bailly Unit 8 Inspection Results Overview



Level 3



Bailly Unit 8 Inspection Results Overview

AIG

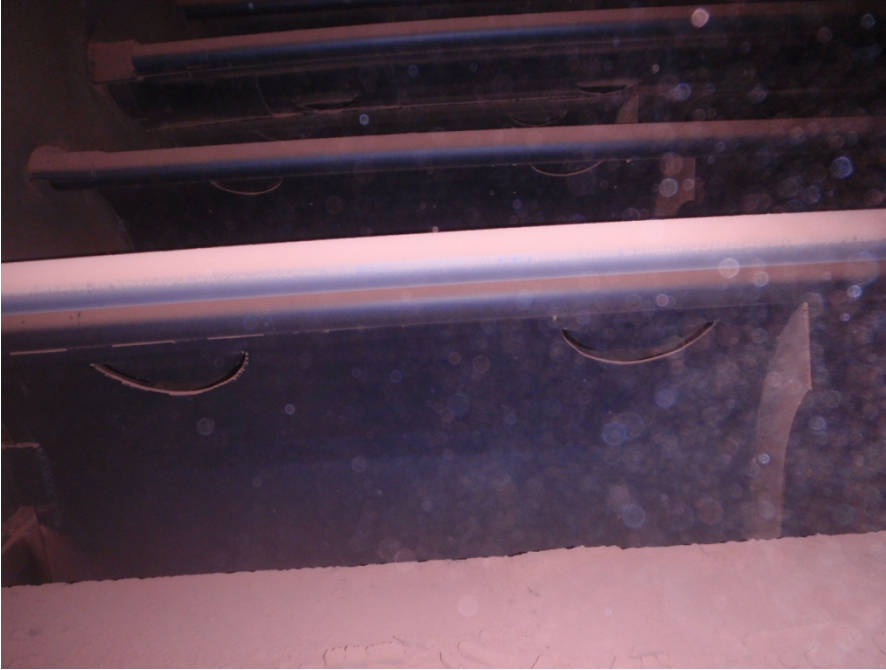


North Side



South Side

Bailly Unit 8 Inspection Results Overview



“Clean” Vanes



Bailly Unit 8 Inspection Results Overview



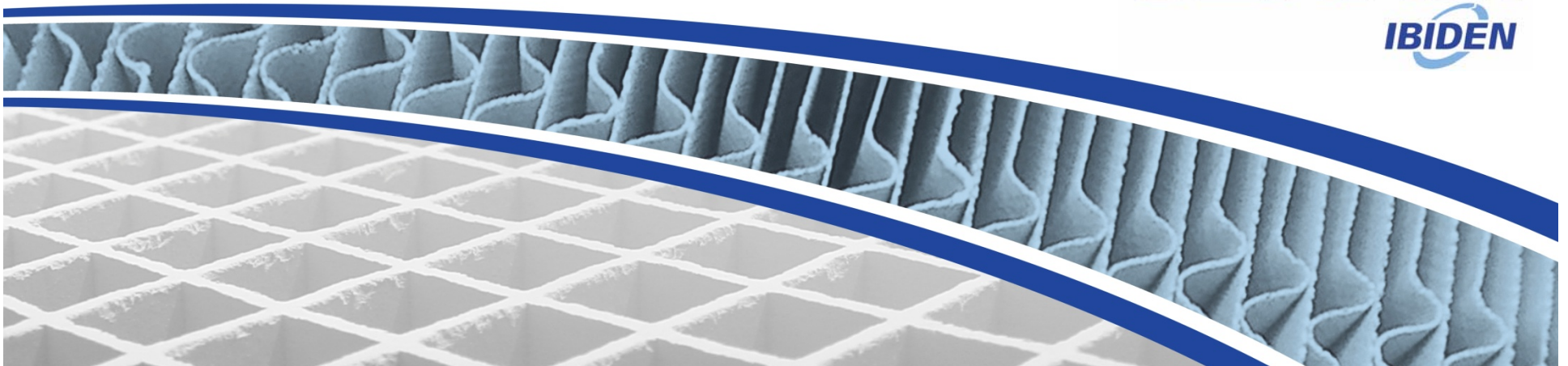
Repair LPA Screen



2013 Reinhold Presentation

NIPSCO Bailly Unit 8 Affects of System Modifications to AIG Tuning

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AIG Tuning Bailly Unit 8

Bailly Unit 8	Baseline	Final
Target Distribution:		
Points within ± 20 ppm	4 of 42	38 of 42
Points within ± 25 ppm	5 of 42	42 of 42

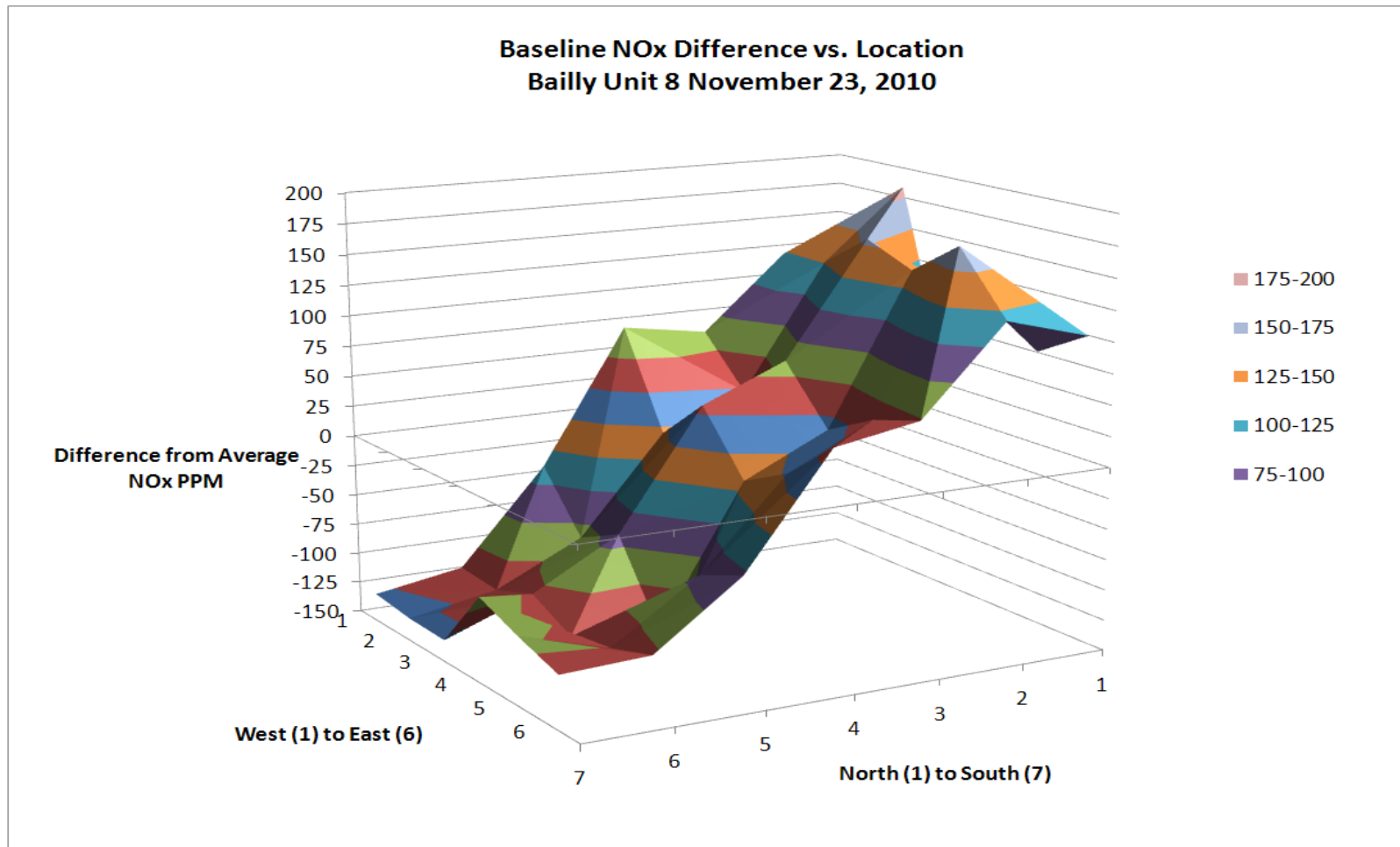
Bailly Unit 8 Baseline SCR Outlet NOx Distribution Results							
1	Grid Pt #	501	504	502	505	503	506
	Deviation (\pm)	99	184	40	102	76	100
2	Grid Pt #	507	510	508	511	509	512
	Deviation (\pm)	124	126	155	139	168	119
3	Grid Pt #	513	516	514	517	515	518
	Deviation (\pm)	63	23	61	16	37	49
4	Grid Pt #	519	522	520	523	521	524
	Deviation (\pm)	74	-4	32	-17	3	37
5	Grid Pt #	525	528	526	529	527	530
	Deviation (\pm)	-37	-84	-66	-130	-68	-52
6	Grid Pt #	531	534	532	535	533	536
	Deviation (\pm)	-115	-118	-105	-123	-115	-103
7	Grid Pt #	537	540	538	541	539	542
	Deviation (\pm)	-127	-131	-132	-80	-94	-106

AIG Tuning Bailly Unit 8 (Rebalancing)

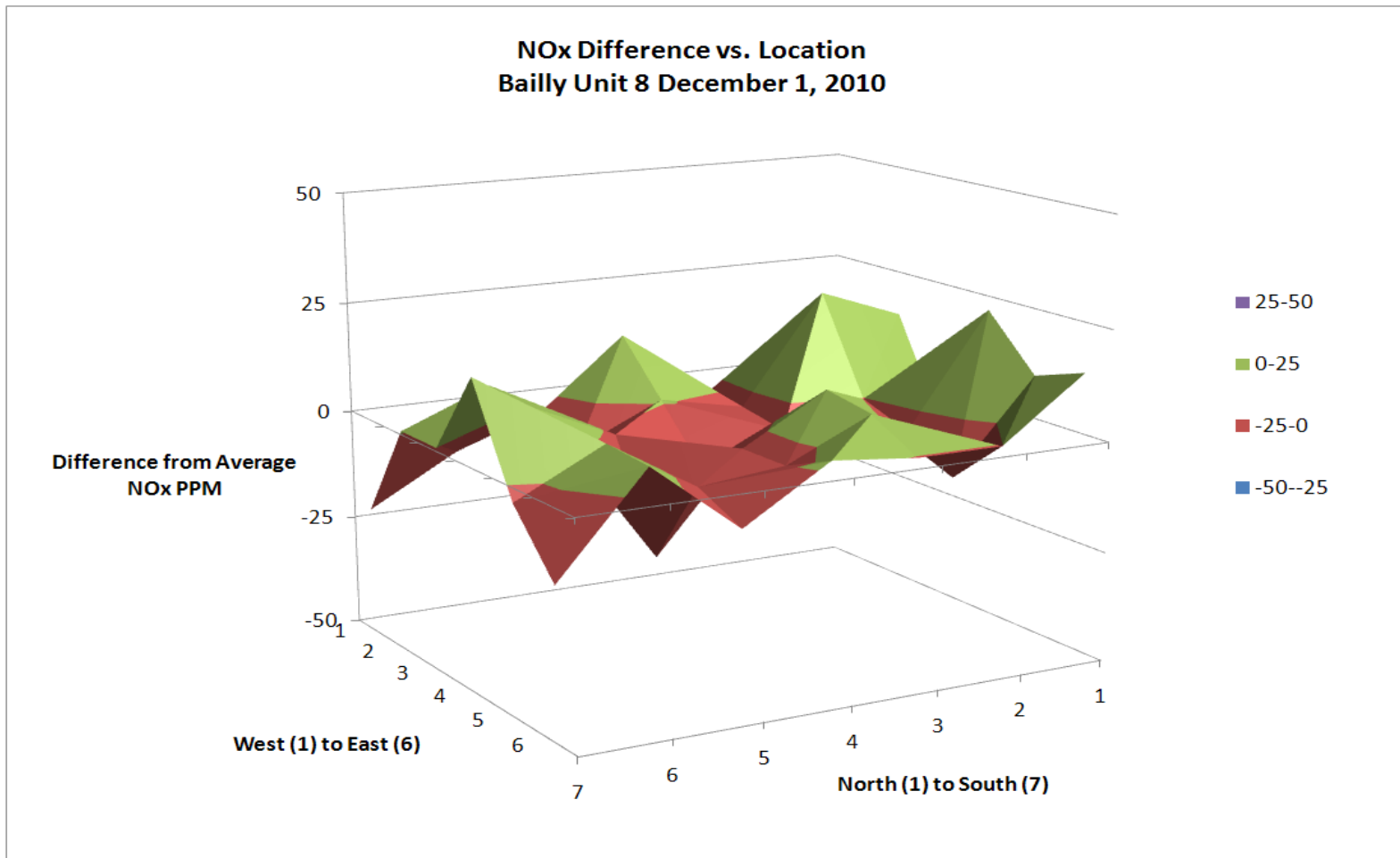
Bailly Unit 8	Baseline	Final
Target Distribution:		
Points within ± 20 ppm	4 of 42	38 of 42
Points within ± 25 ppm	5 of 42	42 of 42

Bailly Unit 8 Final SCR Outlet NOx Distribution Results							
1	Grid Pt #	501	504	502	505	503	506
	Deviation (\pm)	7	15	-8	22	10	14
2	Grid Pt #	507	510	508	511	509	512
	Deviation (\pm)	-12	22	0	-4	-11	0
3	Grid Pt #	513	516	514	517	515	518
	Deviation (\pm)	-4	-3	-5	8	6	0
4	Grid Pt #	519	522	520	523	521	524
	Deviation (\pm)	13	1	-11	-3	-3	2
5	Grid Pt #	525	528	526	529	527	530
	Deviation (\pm)	-3	-8	-1	-25	-5	-10
6	Grid Pt #	531	534	532	535	533	536
	Deviation (\pm)	-10	9	8	3	7	6
7	Grid Pt #	537	540	538	541	539	542
	Deviation (\pm)	-21	1	1	20	-3	-16

AIG Tuning Baily Unit 8



AIG Tuning Bailly Unit 8



AIG Tuning Baily Unit 8

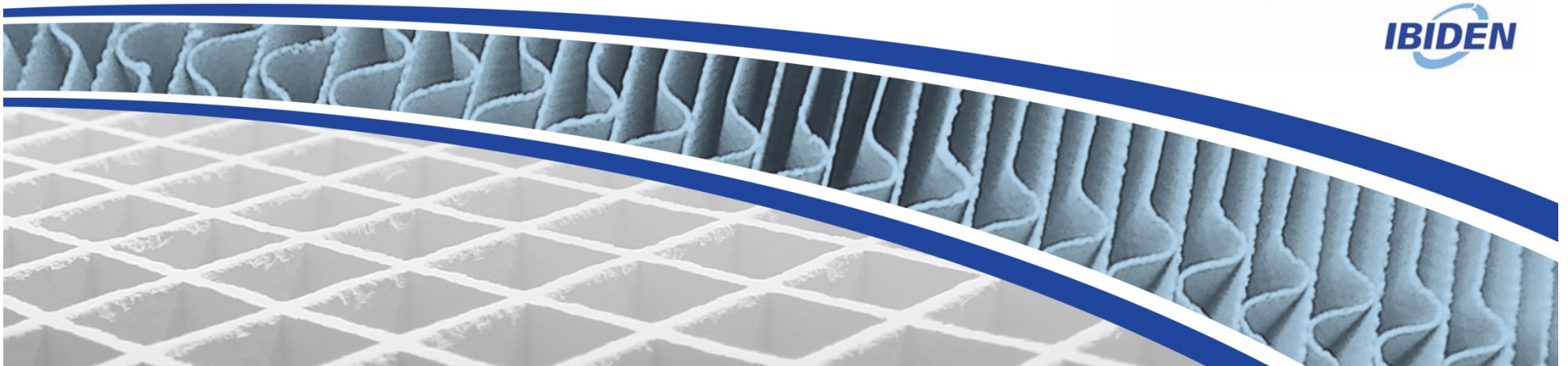
- Pressure Drop Measurements
 - Historically Pressure Taps and Lines Are Plugged.
 - Urea Salt's Out and Plugs Taps and Lines. Maintaining Clean Lines Extremely Difficult
 - Recorded Number of Threads Exposed for All 42 Valves



2013 Reinhold Presentation

NIPSCO Bailly Unit 8 Summary of Modifications and Results

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Bailly Unit 8 Summary

- Annual Reactor Inspection Performed Over Past 8 Years
- Historically Pluggage Observed Due to LPA, Unburned Carbon and Ash Dropout (Velocity Maldistribution)
- Solutions Have Been Developed and Implemented to Eliminate Pluggage
 - Installed STEAG LPA Screen; Screen Stationary; Repair Screen Panels
 - Working to Keep Unburned Carbon Levels Lower
 - CFD Modeling Used to Improve Velocity Distribution
 - 43.5% Baseline to 31% With “Novel” Economical Solution (15% Design); Further Changes Possible, But Considered Not Cost Effective
 - Localized High Velocity Areas More Prevalent (Examine CFD & Develop Solution)
 - Installed Larger Pitch to Mitigate Pluggage and Increased Operations/Fuels Flexibility
 - Reactor Pressure Drop Substantially Lower (7 in. w.g. vs. 3 in. w.g.)
 - Pressure Drop Lower From Decomposition Chamber to AIG

Thank You!

Questions?

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